

# Advancement of LED-Based Hazardous Gas Sensors for Space Applications

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# Agenda



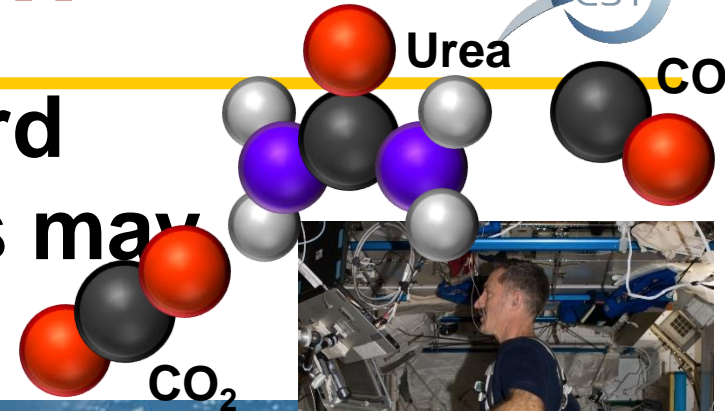
- Motivation
- Technical Background
- High Altitude Balloon Flight
- Swept Grating Design
- Sensor Testing
- Laser Validation
- Conclusions
- Future Work
- Acknowledgements

# Need For Sensors & Design Theory

# Motivation

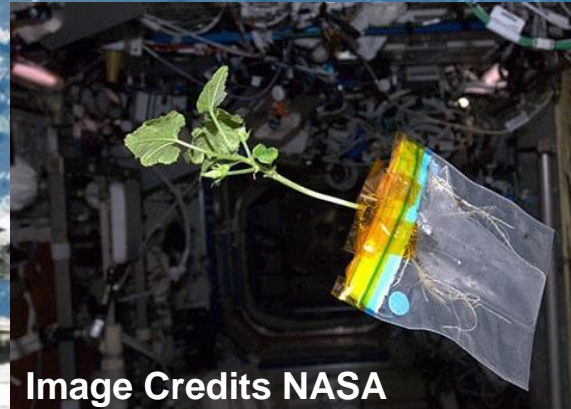


- Cabin air is confined aboard spacecraft and toxic gases may accumulate

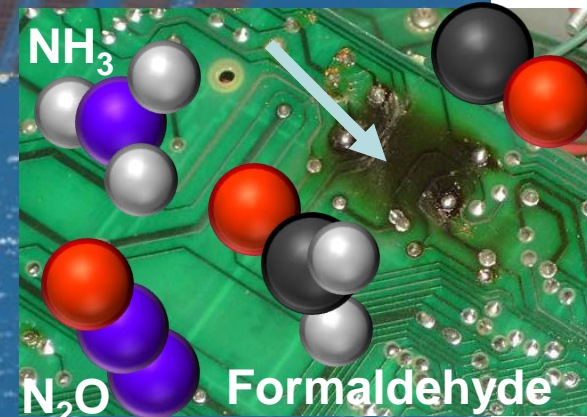
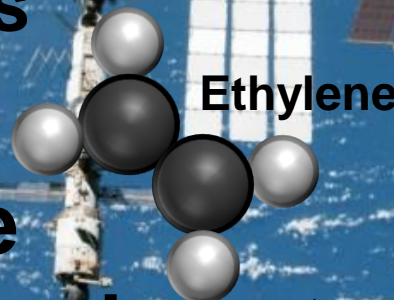


- Toxic gas sources include

- Human activity
- Astroculture
- System malfunctions



- Rapid detection is necessary to ensure safety of crew & experiments



# Motivation

- **Many current hazardous gas detection sensors are particle based**
  - Particle ionization smoke detector
  - NIR laser forward scattering particle detector
- **LEDs are more durable and less expensive than lasers**

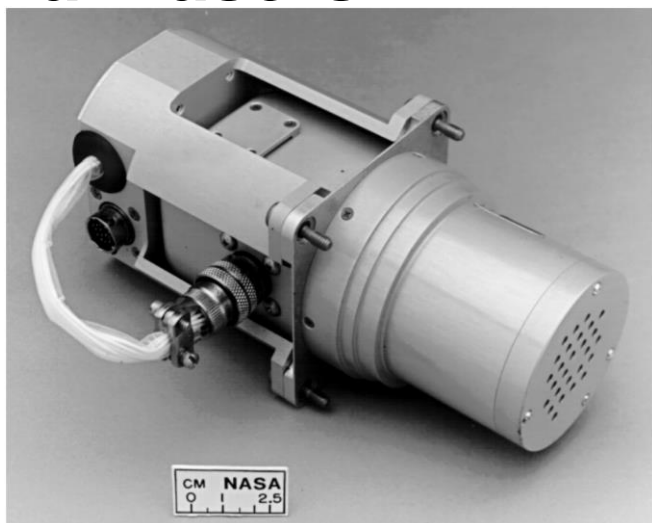


Image Credits NASA

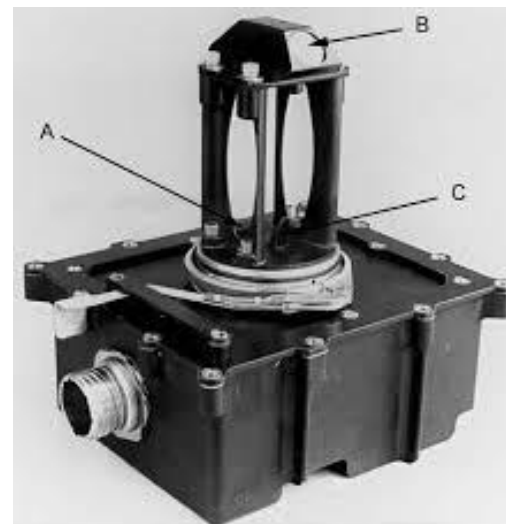


Image Credits NASA

# Absorption Spectroscopy & Beer's Law

- Absorption Spectroscopy is an application of the Beer-Lambert Law:

$$A(\lambda) = -\ln\left(\frac{I_\lambda}{I_{\lambda,0}}\right) = \sum_i \int_{s_j}^{s_{j+1}} k_\lambda \cdot x_i ds$$

$A(\lambda)$  - Spectral absorbance

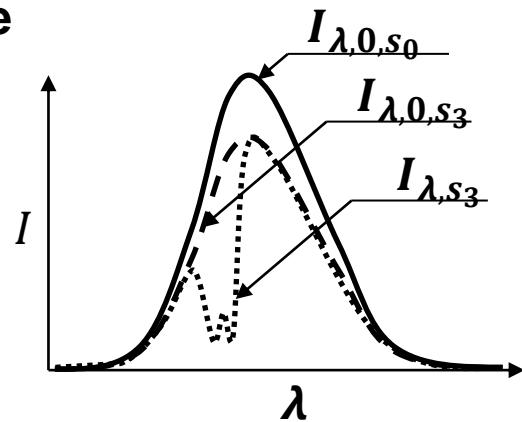
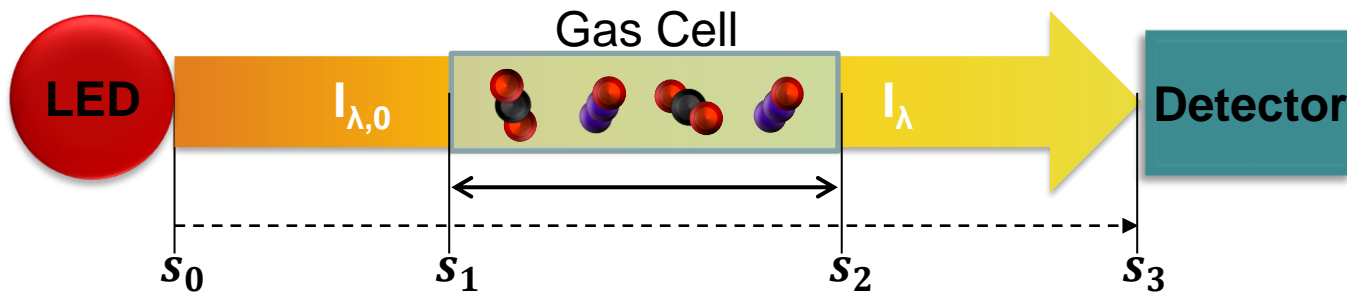
$x_i$  - Molar fraction of  $i^{\text{th}}$  species

$I_{\lambda,0}$  - Incident spectral intensity of electromagnetic radiation

$k_\lambda$  - Spectral absorbance coefficient (function of pressure, temperature, & species)

$I_\lambda$  - Transmitted spectral intensity of electromagnetic radiation

$s$  - Path variable

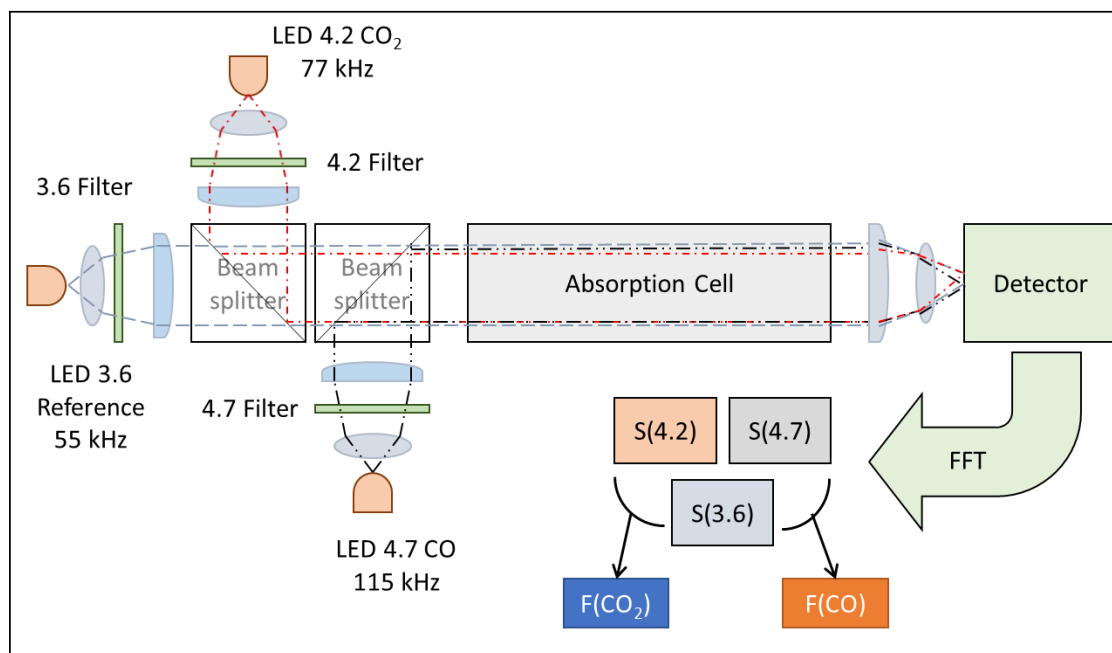


# Sensor History

# High Altitude Balloon Flight

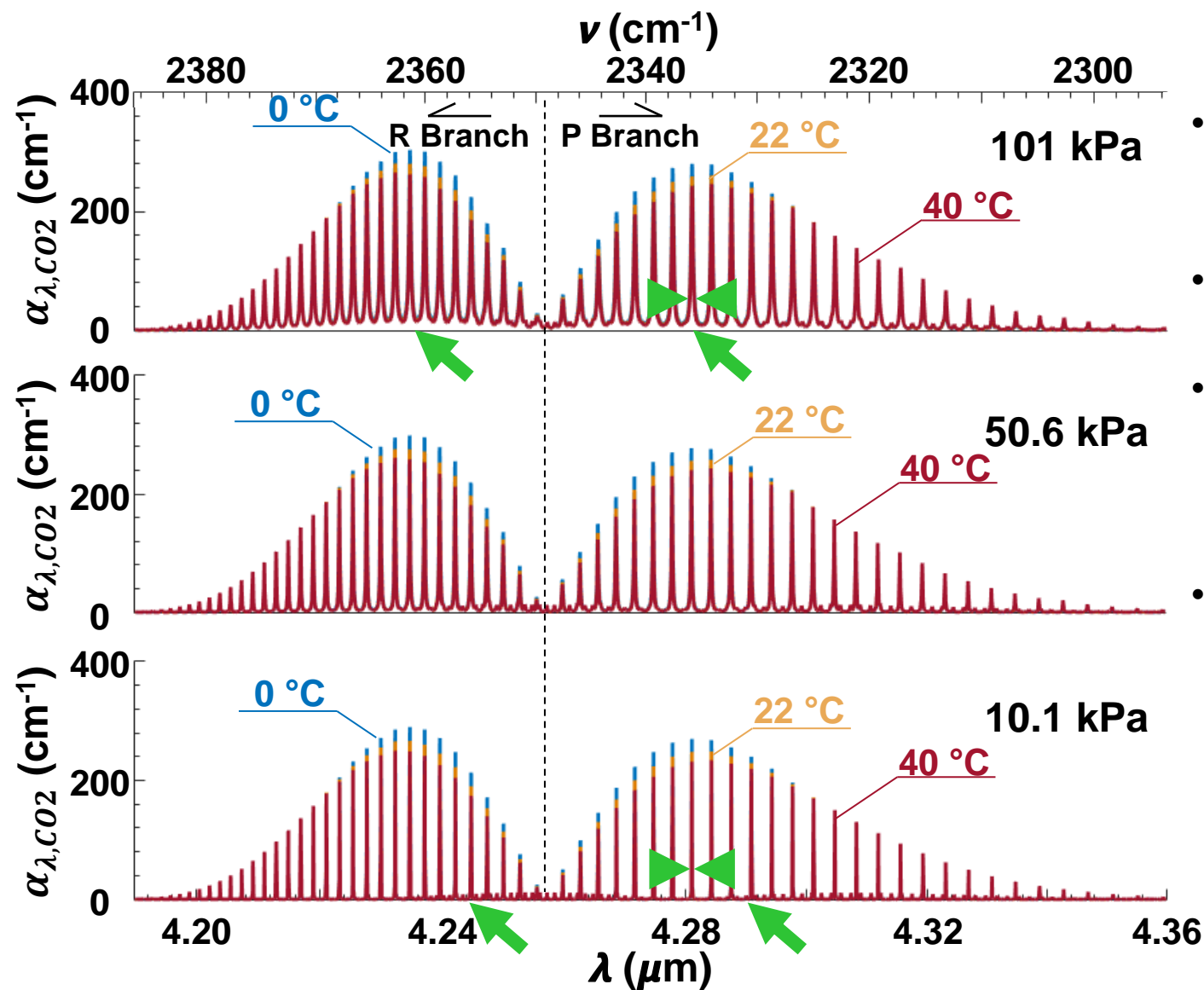


# Original Design



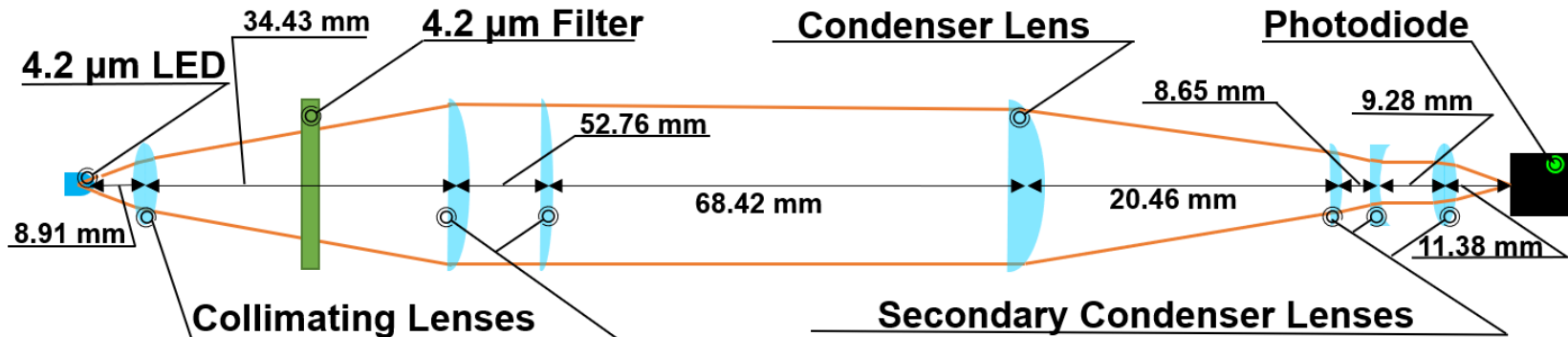
- **3 LEDs: CO<sub>2</sub>, CO, and reference**
- **Modulated at different frequencies**
- **Separated signals via Fast Fourier Transform (FFT)**
- **Autonomous operation using a National Instruments cRIO DAQ**

# Abridged Sensor Overview

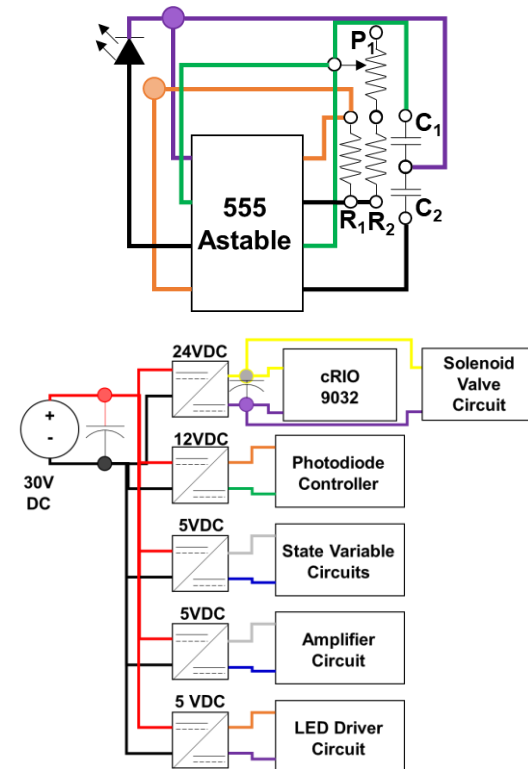


- Temperature dependent feature distribution
- As pressure ↓, peak width narrows
- As pressure ↑ baseline absorbance is present
- Baseline effects cause saturation when used in conjunction with broadband source

# Abridged Sensor Overview

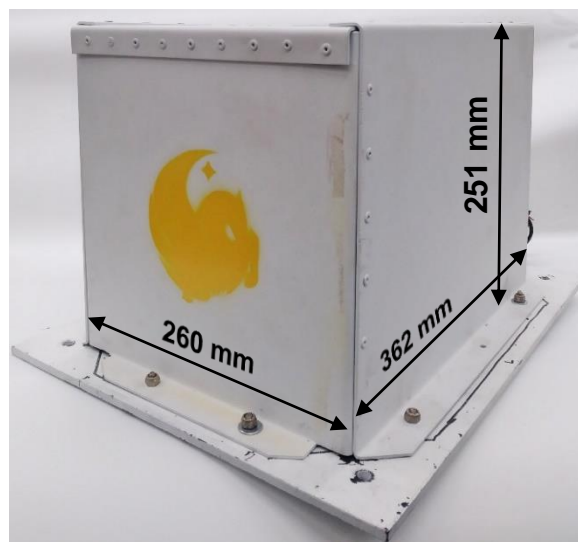
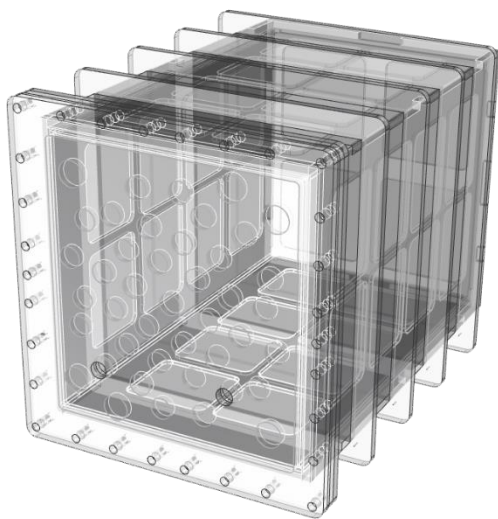


- **Single LED used with filter for CO<sub>2</sub> detection**
  - Reduction in complexity from previous design
  - Omitted reference LED
- **Designed open-loop LED driver**
  - Ceramic capacitor to allow temperature-dependent frequency changes
- **Isolated power distribution channels**
- **Autonomous operation using a National Instruments cRIO DAQ**



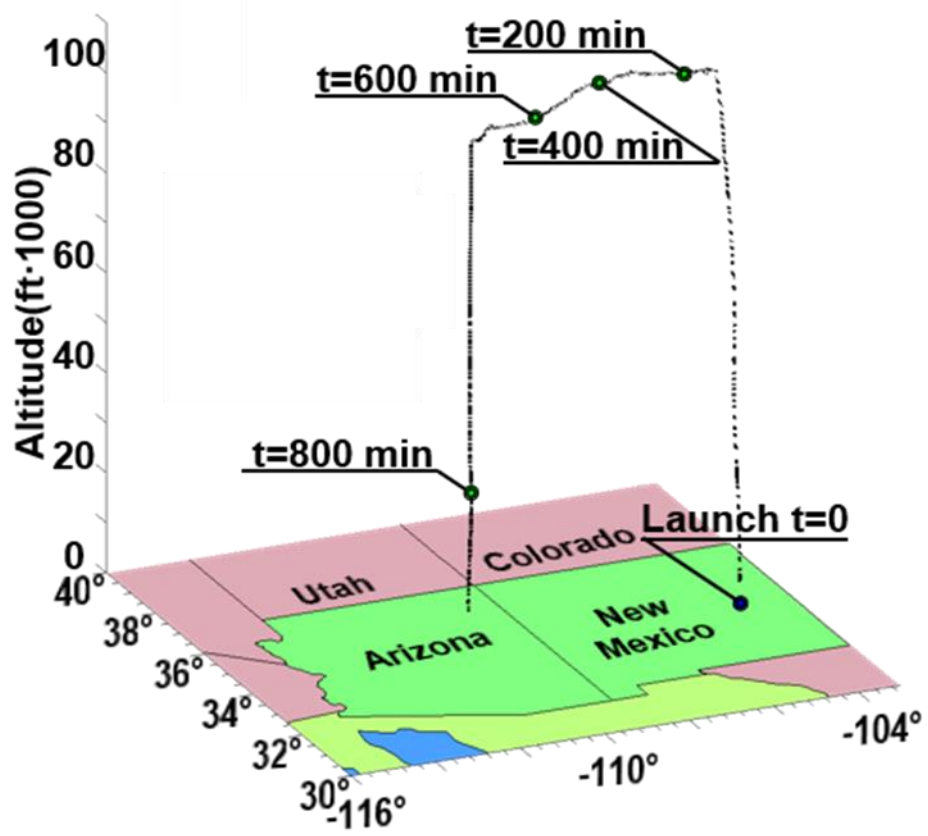
# Sensor Enclosure & Packaging

- **Components placed in acrylic enclosure**
  - Panels cut using laser CNC & assembled using acrylic monomer
  - Ribs and layered design used to ensure lightweight construction
- **Acrylic enclosure sealed using greased butyl gasket**
  - Passthroughs on the enclosure for electrical signals & power
- **Aluminum housing surrounding acrylic for protection**
  - High altitude solar heating &  $\mu$ wave interference

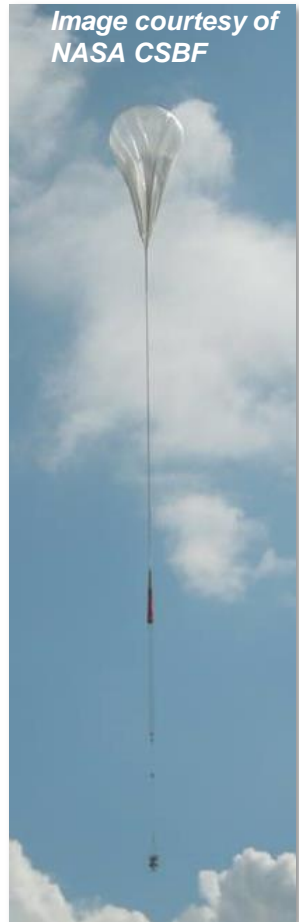


# Balloon Flight

- NASA Columbia Scientific Balloon Facility Ft. Sumner, NM
- Sensor packaged and mounted on balloon payload
- Autonomous operation test
- Enclosure sealed with ambient air
- Power supplied via NASA HASP Platform



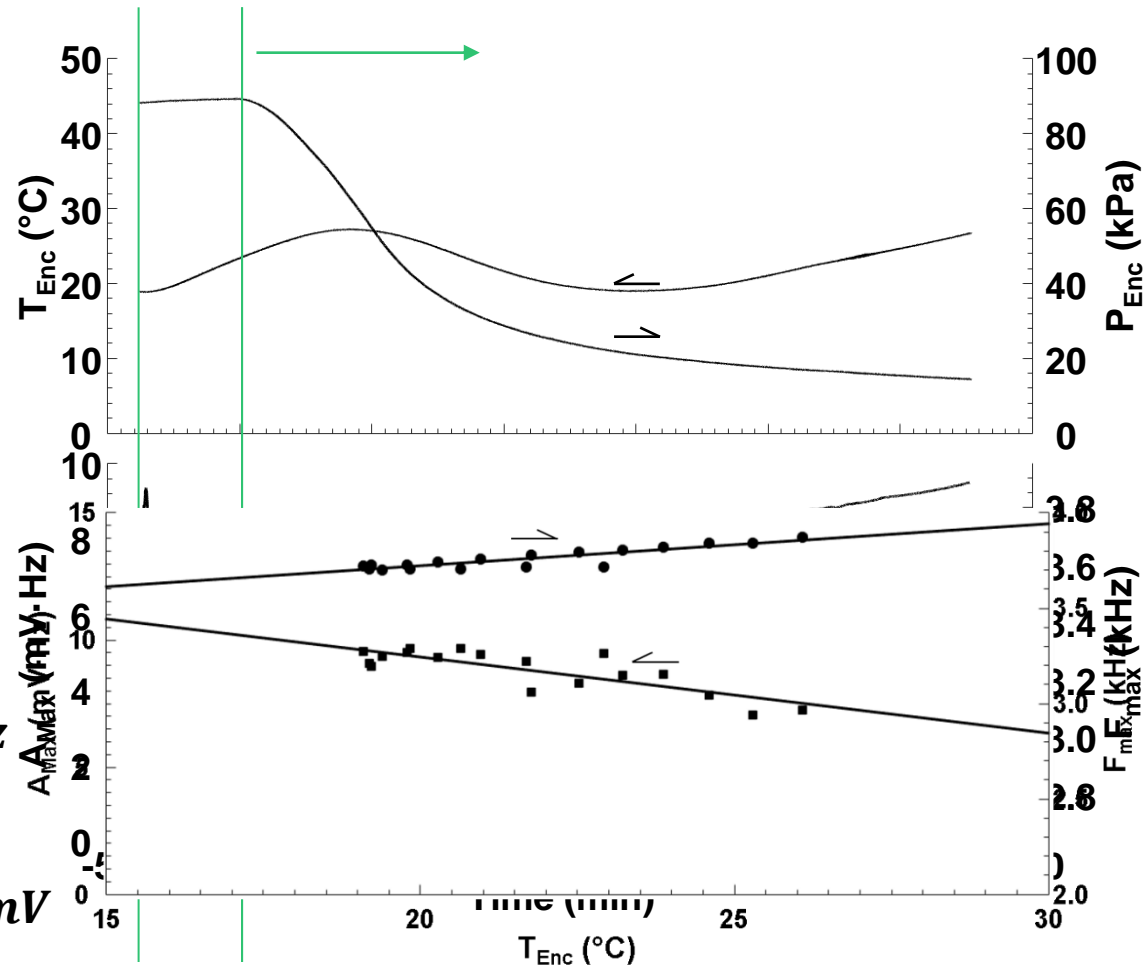
Max Altitude: 109,412 ft  
 Nominal Float Altitude: 105,000 ft  
 Launch Time: 9/4/2017 14:04:25 UTC  
 Duration: 776 min.



# Autonomous Flight Data



- Intensity, temperature & wave center changing
- Following warmup
  - Signal intensity & Frequency correlate with temperature
- Curve fits for baseline detection were then fit
  - Temperature dependent



$$F_{max}(T^{\circ}C) = 0.022 \text{ kHz}/^{\circ}C \cdot T(^{\circ}C) + 3.283 \text{ kHz}$$

$$A_{max}(T^{\circ}C) = -0.299 \text{ mV}/^{\circ}C \cdot T(^{\circ}C) + 15.313 \text{ mV}$$



# Balloon Flight Conclusions



- **Simplified design requiring less power and optical space**
- **Proved functional and able to withstand high-altitude balloon flight**
- **Established effect of temperature on modulated frequency**
- **Expand detection range without greatly increasing optical complexity**

# Swept Grating Sensor

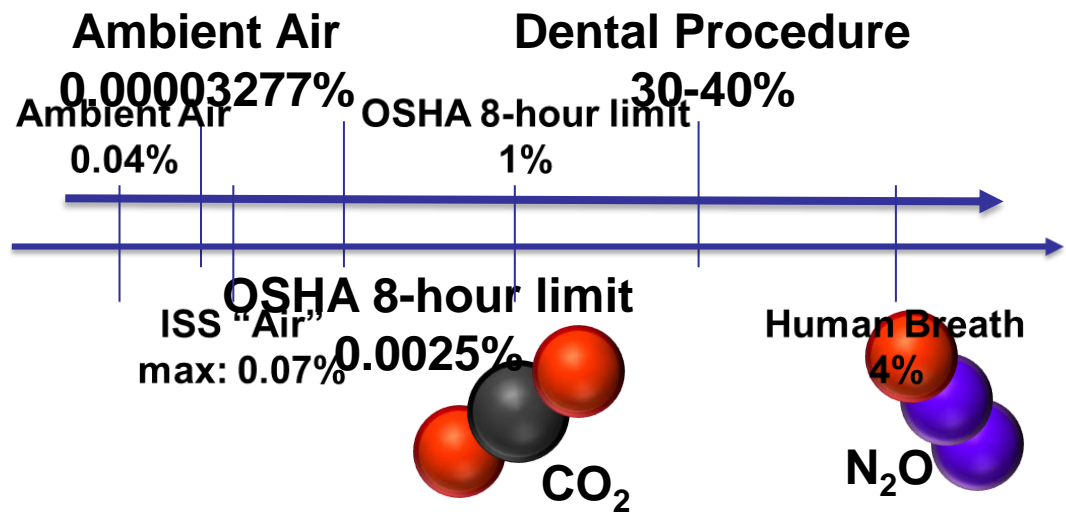




# Sensor Target Gases



- **CO<sub>2</sub>**
  - Released during combustion and smoldering events
  - Impairs cognitive capacity in large concentrations
- **N<sub>2</sub>O**
  - Oxidizer in hybrid rockets
  - Sedative and affects critical thinking



Main symptoms of

**Volume in air Legend:**

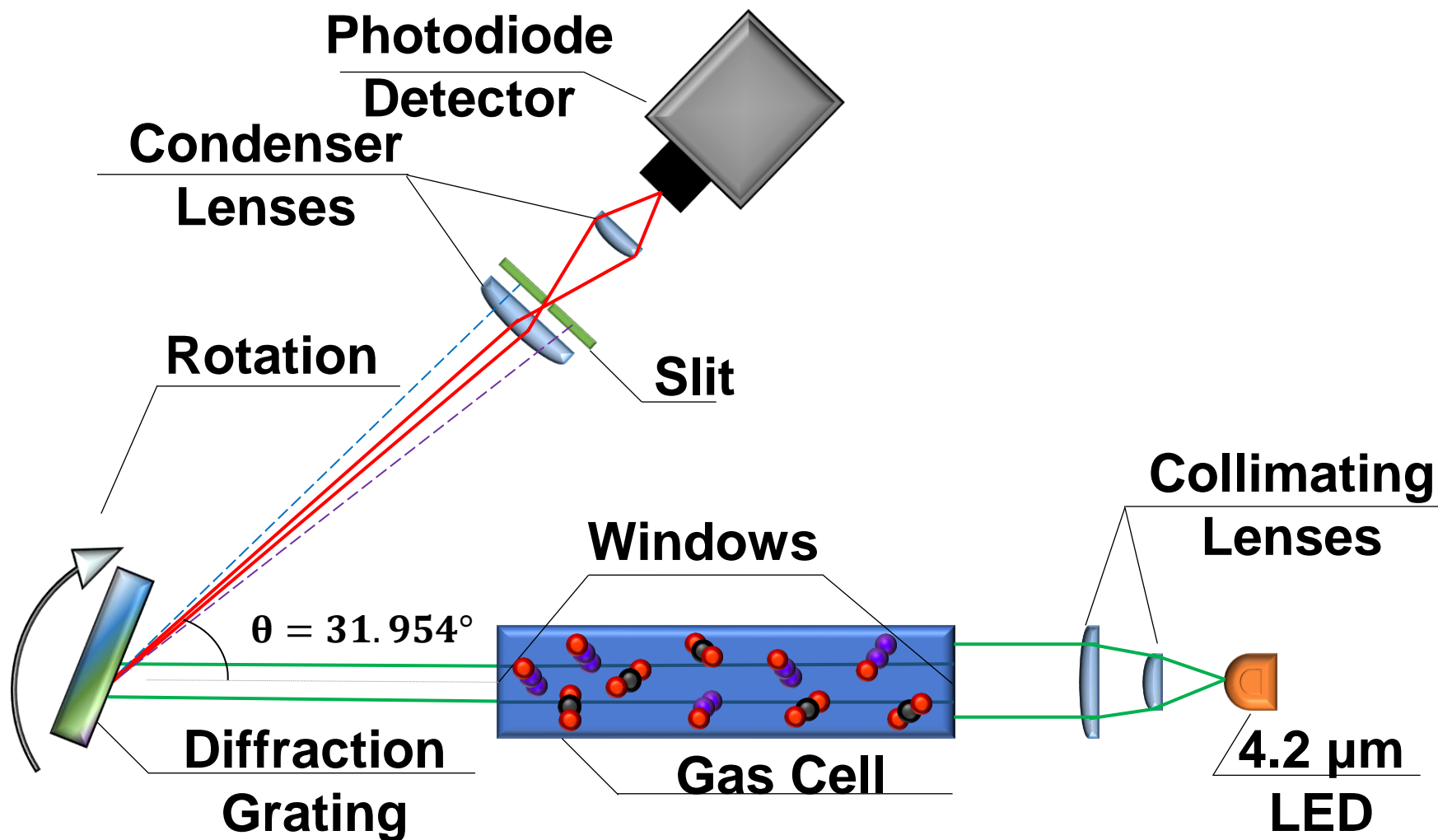
- 1%
- 3%
- 5%
- 8%

**Symptoms:**

- Respiratory - Shortness of breath
- Muscular - Tremor
- Skin - Sweating
- Increased heart rate and blood pressure

Source: [www.CO2meter.com](http://www.CO2meter.com)

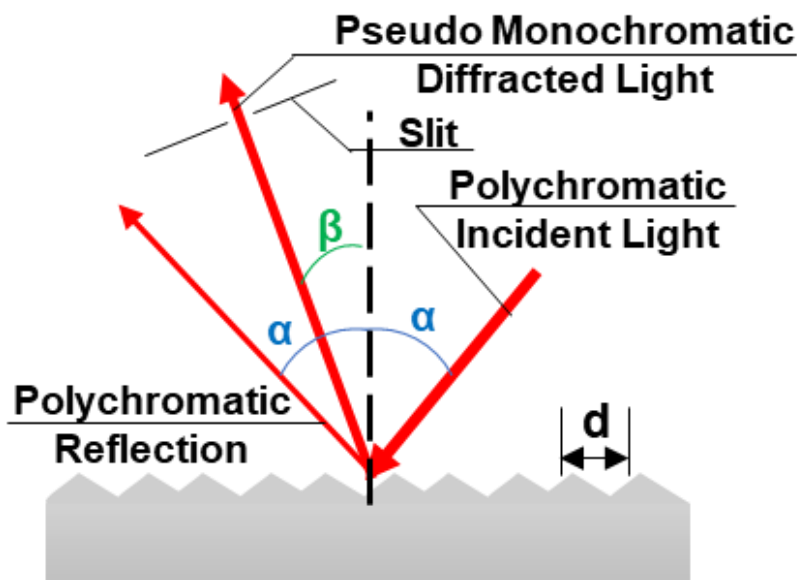
# Optical Path



# Diffraction Grating

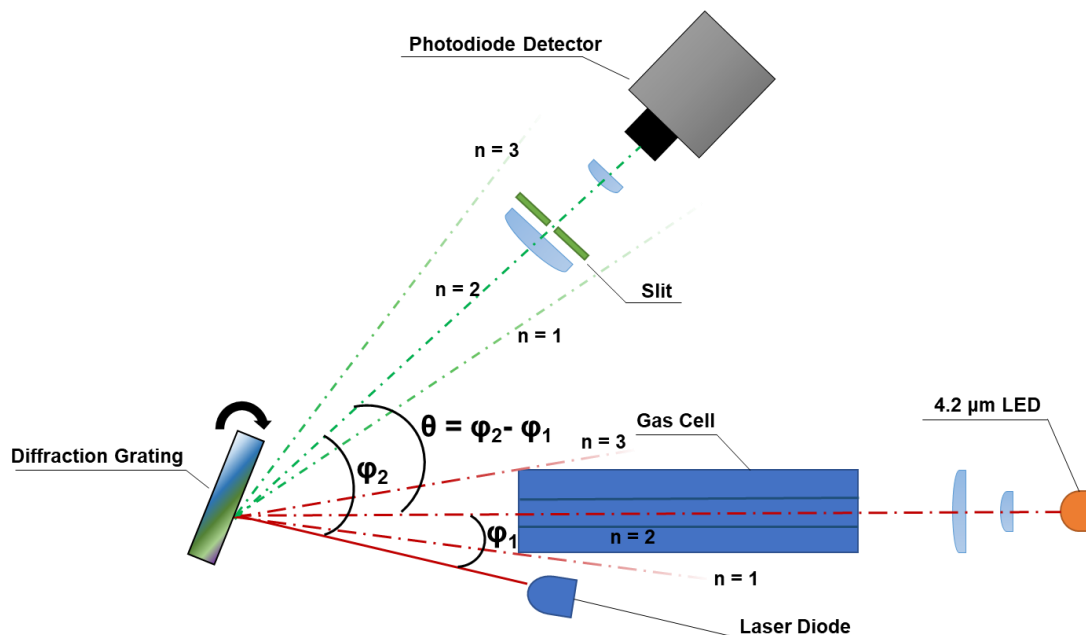
- Detected wavelength calculated using grating equation:

$$n\lambda = d[\sin(\alpha) \pm \sin(\beta)]$$



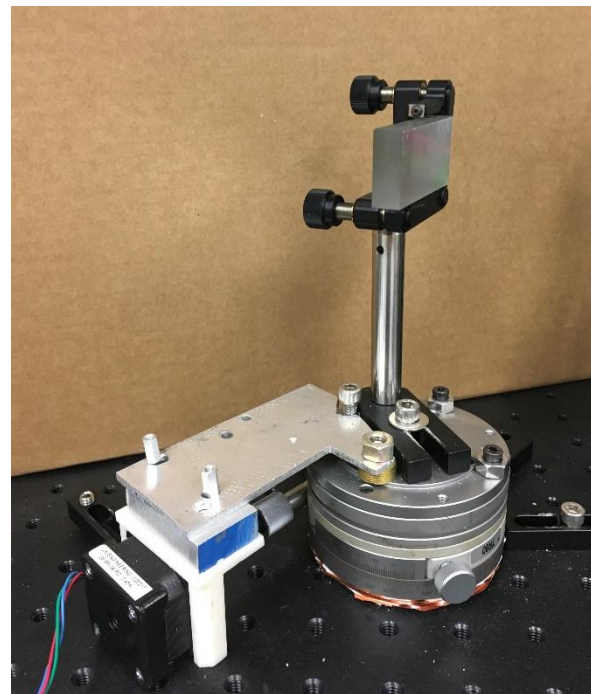
# Grating Calibration

- **Grating “zero” reference**
  - Laser diode placed perpendicular to grating
  - Measuring distance between adjacent modes
  - $n\lambda = d[\sin(\alpha) \pm \sin(\beta)]$



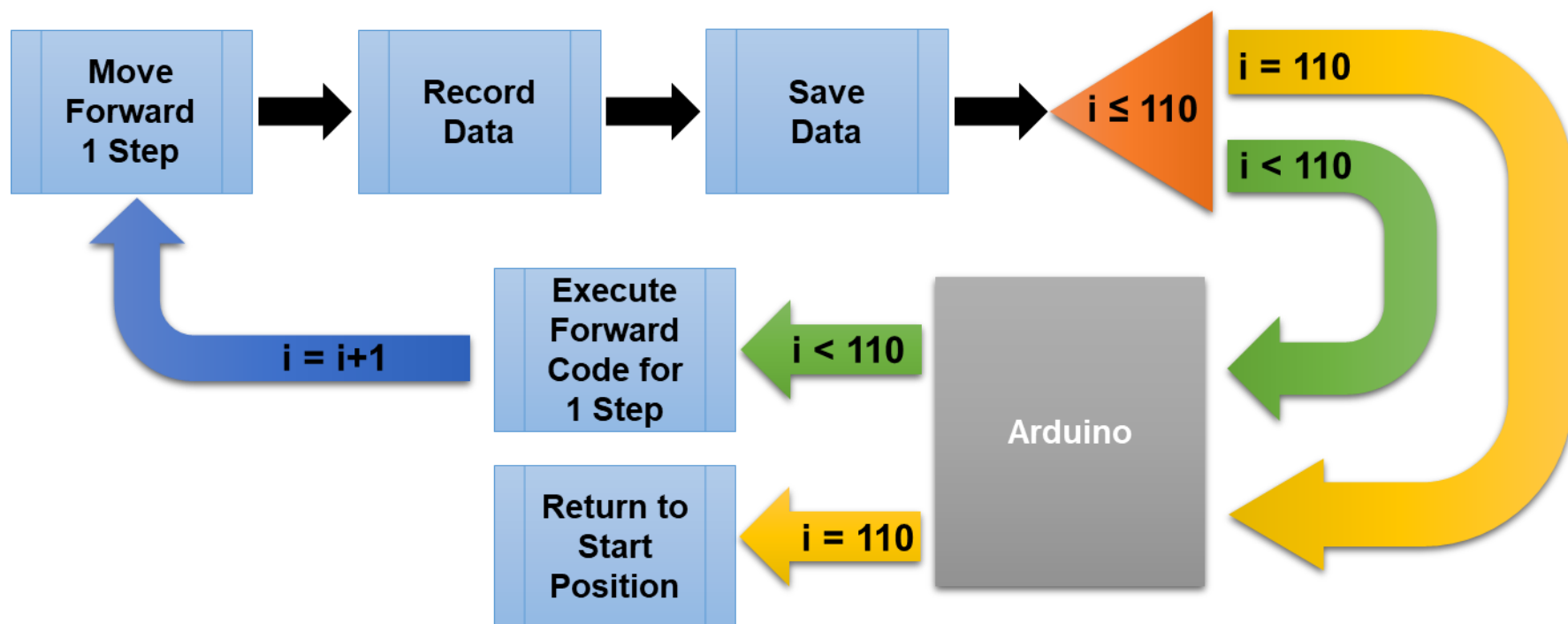
# Grating Calibration

- **For valid measurements, a repeatable grating position is necessary**
  - **Stepper motor used for actuation**
  - **Motor driving function parametrically investigated for minimal drift**



# Grating Calibration

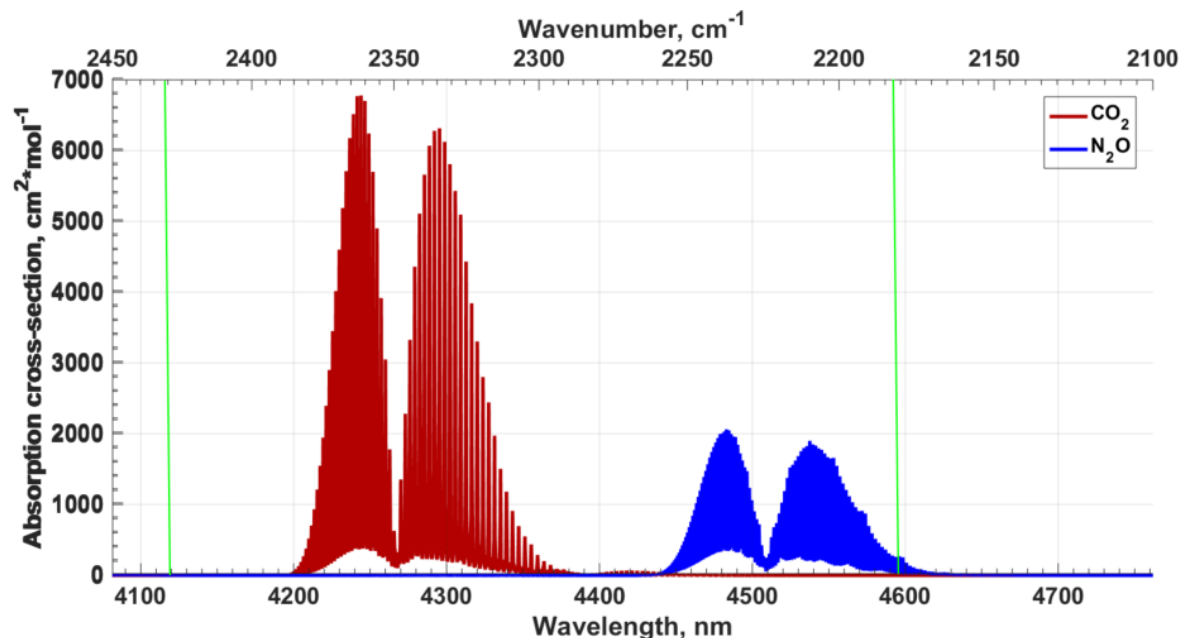
- DAQ controls the movement of the grating in a uniform manner



# Measurement Sweep Range

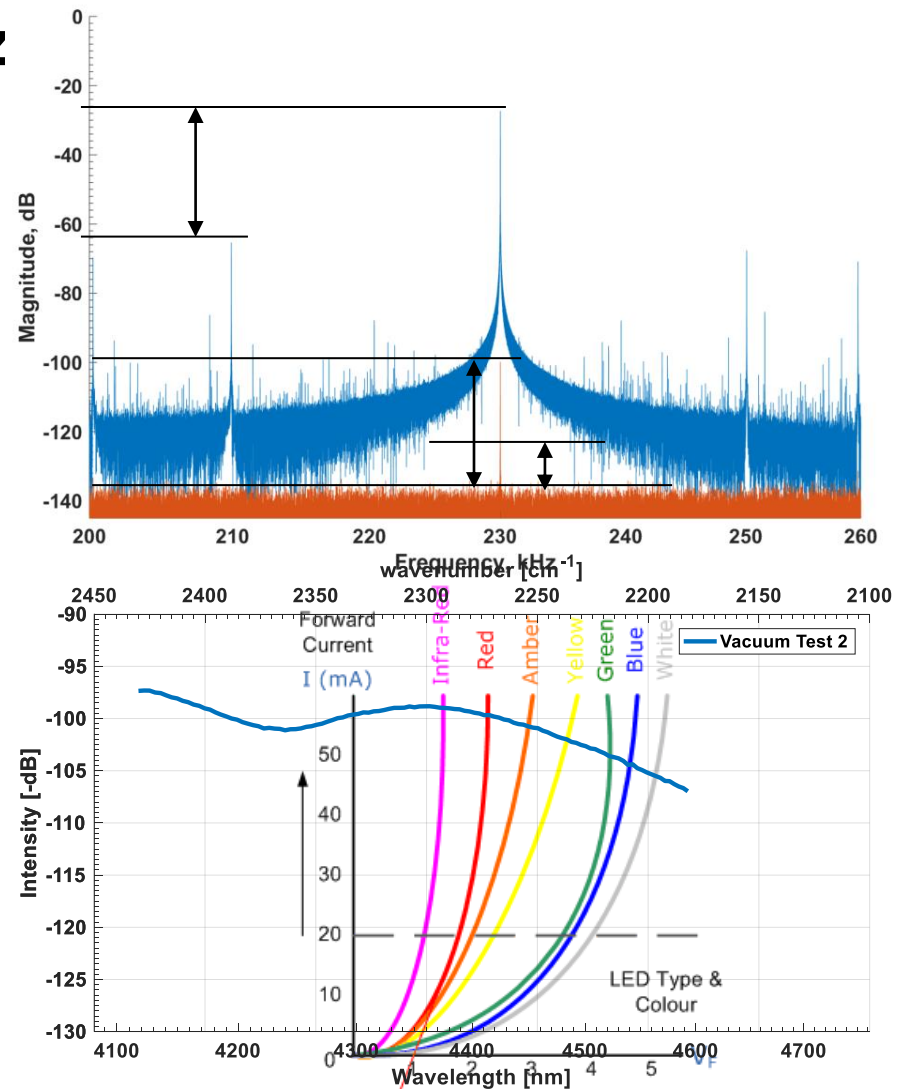


- **Wavelength Range: 4117nm – 4592nm**
  - Split into 110 discretizations
  - Step size of 4.318nm



# Signal Collection & Interpretation

- LED modulated at 250 kHz to reduce noise
- FFT & Absorbance
  - Figure shows FFT at 4185nm for vacuum
  - Save peak signal and reference data (110)
  - $P_{signal,dB} = 10 \log_{10} \left( \frac{P_{signal}}{P_{ref.}} \right)$
  - $A(\lambda) = -\ln \left( \frac{I_{\lambda}}{I_{\lambda,0}} \right)$ 
    - $I_{\lambda}$  = test detector signal
    - $I_{\lambda,0}$  = vacuum detector signal
- $SNR_{dB} = P_{signal,dB} - P_{noise,dB}$ 
  - $SNR_{dB,ref} = 37dB$
  - $SNR_{dB} = 39dB$

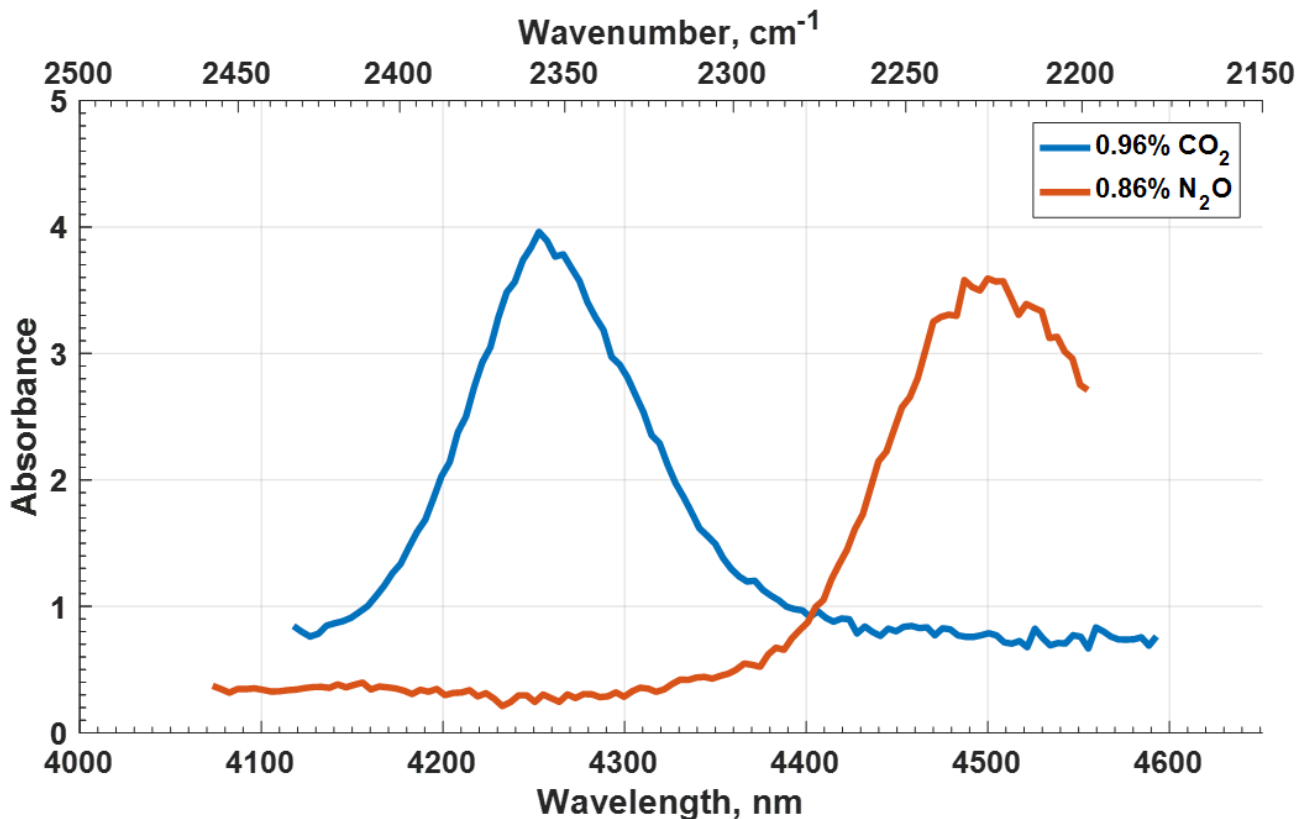




# Cross-Interference Study



- Interference between the two species must be studied before making combined mixtures
- False baseline absorbance is present



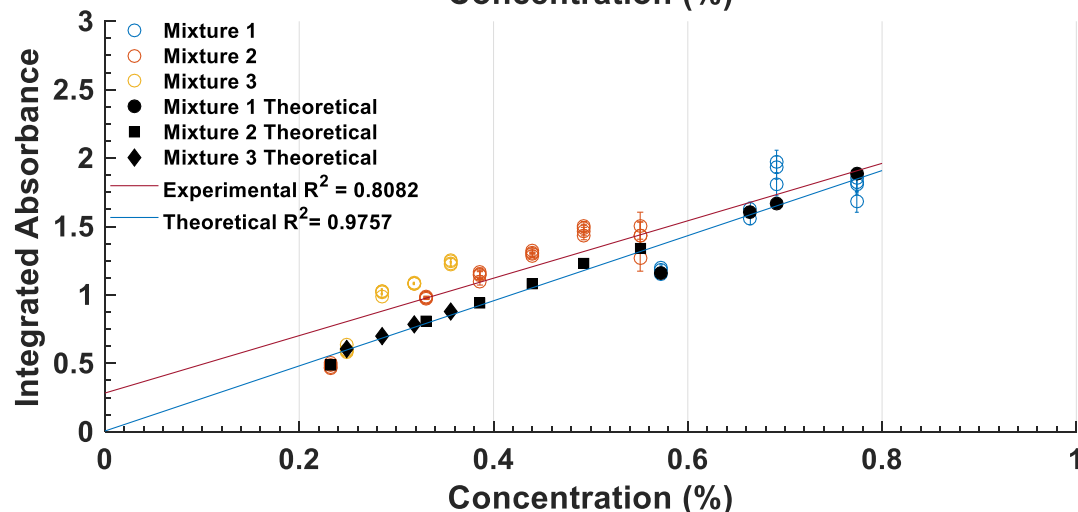
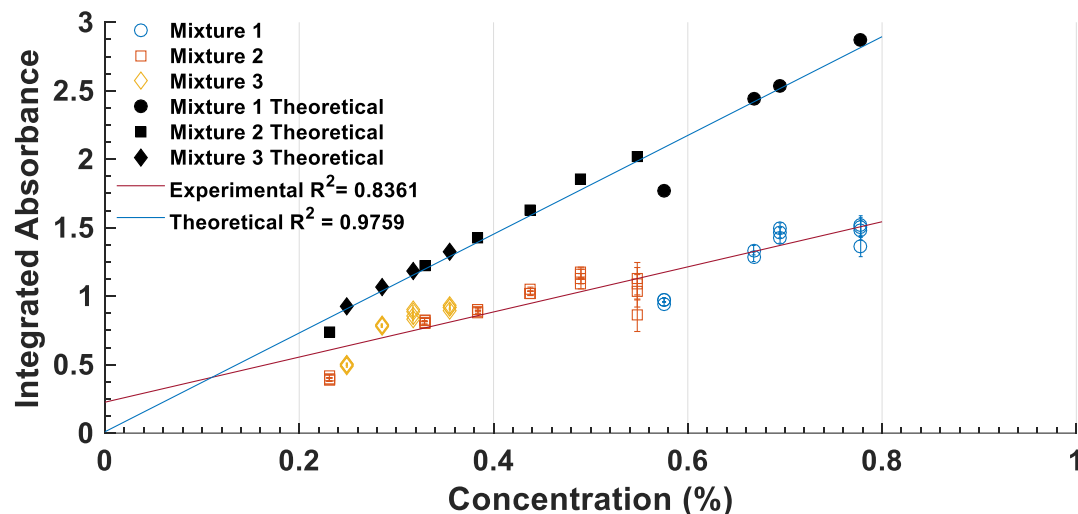


# Test Mixtures

- Mixtures were prepared in a manifold using an MKS Baratron
- All mixtures contained equal concentrations of CO<sub>2</sub> and N<sub>2</sub>O
- The gas cell was filled with the specific mixture and diluted with N<sub>2</sub> to reach different concentrations
- Each test was completed 3-4 separate times
- The gas cell was vacuumed to 0.30 Torr in between experiments

Mixture	Percentage of CO <sub>2</sub> (%)	Percentage of N <sub>2</sub> O (%)	Percentage of N <sub>2</sub> (%)
1	0.778	0.774	98.5
2	0.548	0.551	98.9
3	0.355	0.356	99.3

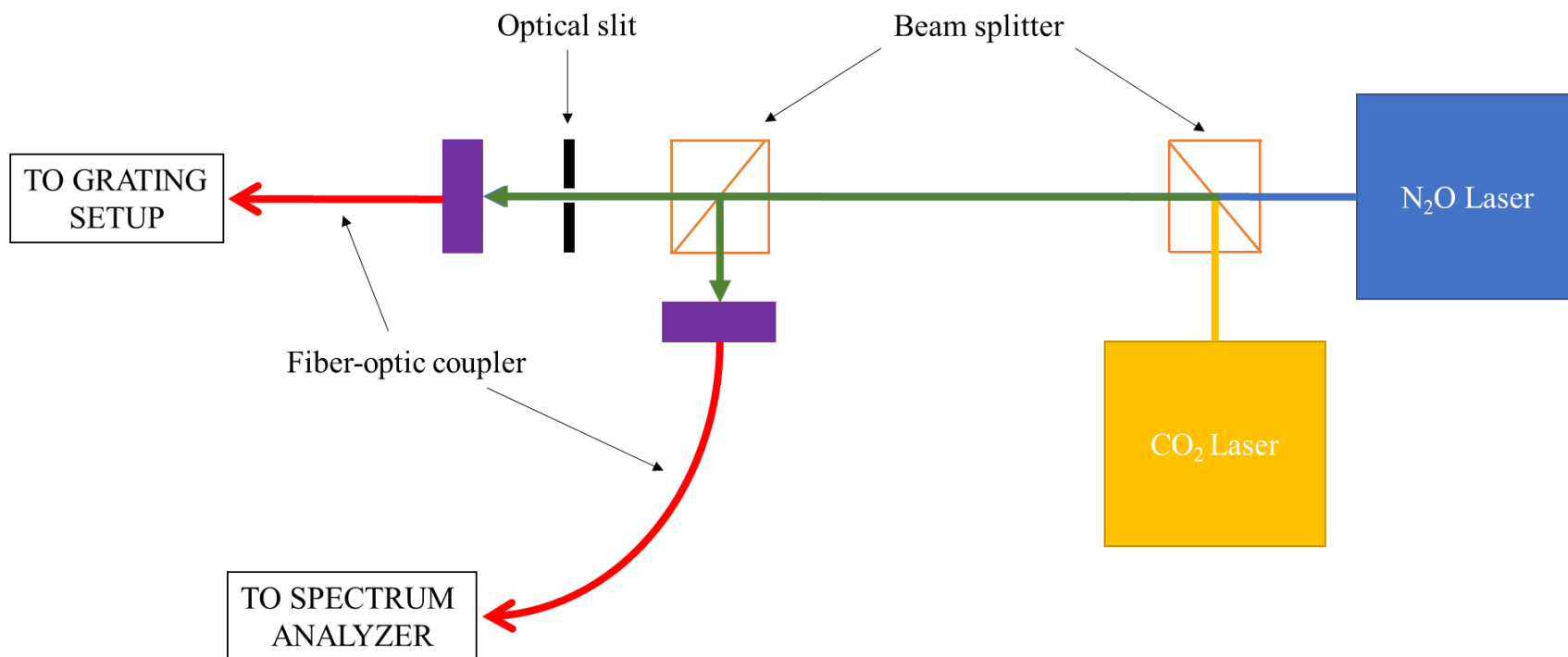
# Integrated Absorbance



- Top figure shows  $\text{CO}_2$  integrated from 4150 to 4350nm
- Bottom figure shows  $\text{N}_2\text{O}$  integrated from 4420 to 4585nm
- HITRAN absorption cross-section modeled using a Gaussian App. Function with an App. Resolution of  $35 \text{ cm}^{-1}$
- Error bars show standard deviation at each concentration value

# Laser Validation Setup

- Validation with 2 Distributed Feedback Quantum Cascade Lasers (QCL)
- “CO<sub>2</sub> Laser” : 4.256 – 4.266μm
- “N<sub>2</sub>O Laser” : 4.583 – 4.596μm





# Laser Test Mixtures



- Mixtures were prepared in the same manner as the LED experiments

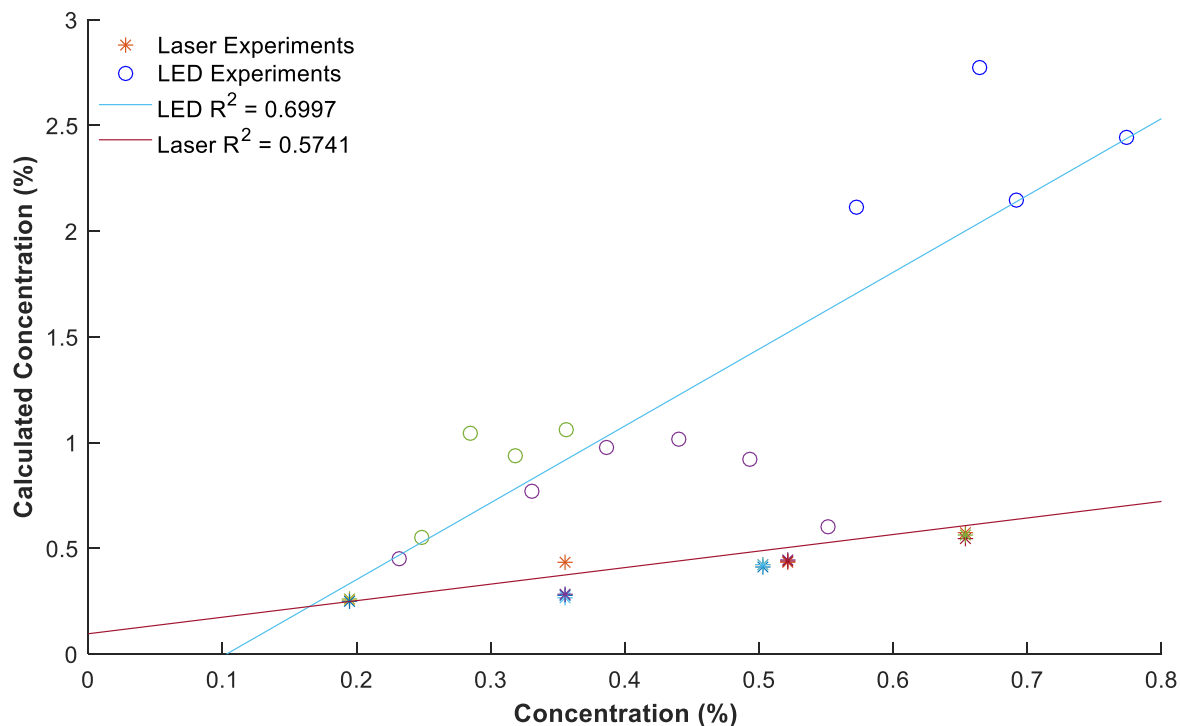
Mixture	Percentage of CO <sub>2</sub> (%)	Percentage of N <sub>2</sub> O (%)	Percentage of N <sub>2</sub> (%)
1	0.355	0.356	99.29
2	0.674	0.654	98.67
3	0.518	0.503	98.97
4	0.537	0.521	98.94
5	0.201	0.195	99.60



# Concentration Comparison



- N<sub>2</sub>O laser at 4589.699 nm
- LED data at same wavelength
- Calculated concentration values from Beer-Lambert Law





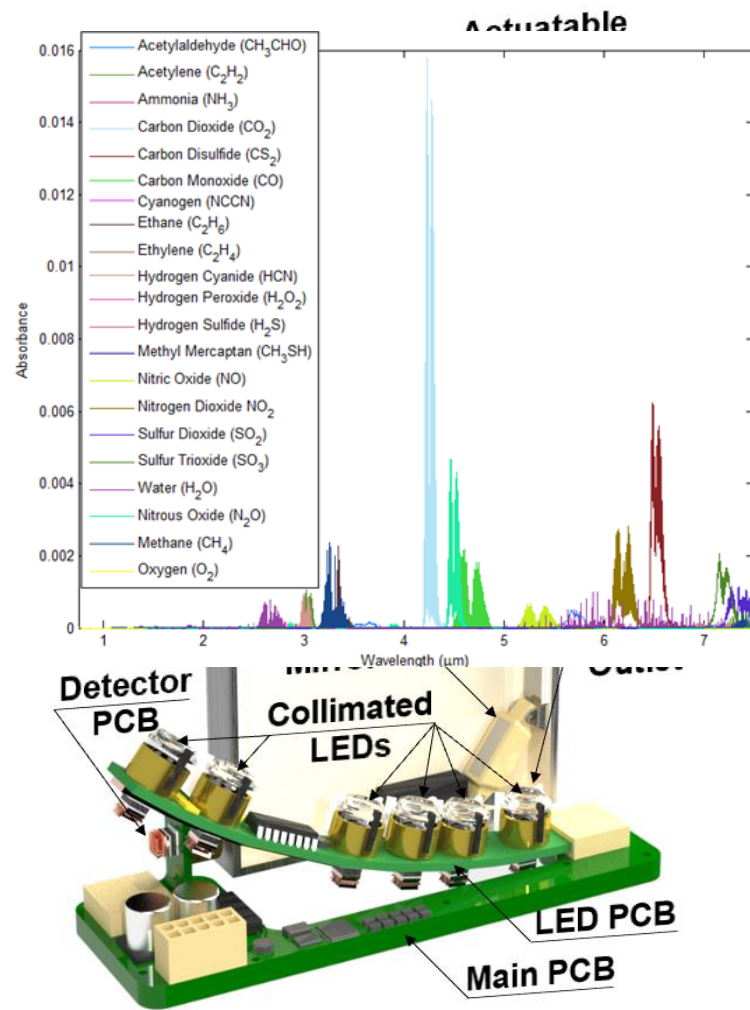
# Conclusions

- **An LED based gas sensor was tested for its abilities to detect toxic compounds**
- **Grating design proved functional for detection of both CO<sub>2</sub> and N<sub>2</sub>O with a single LED**
- **Comparison with laser-based measurements validates the sensor at lower concentrations**
- **Show potential for greatly reducing complexities of gas detection systems**
- **Lead to increased safety in space vehicles**



# Future Work

- Focus on increasing wavelength test range
- Detect more hazardous gases, such as CO
- Conduct tests in harsher environments
- Partner with Commercial Space companies
- Seek other applications and resources (e.g., NASA planetary sensing, environmental applications, etc.)





# Presentations & Publications



- **Journal Publications**

- Akshita Parupalli, Anthony Carmine Terracciano, Zachary Loparo, Justin Urso, S.S. Vasu, “Multi-Species Single-LED Gas Sensor for Space Habitats and Vehicles”, *New Space*, 8(2), 2020.
- Published in Anthony Carmine Terracciano, Kyle Thurmond, Michael Villar, Akshita Parupalli, Justin Urso, Erik Ninnemann, S.S. Vasu, “Hazardous Gas Detection Sensor Using Broadband Light-Emitting Diode-Based Absorption Spectroscopy for Space Applications”, *New Space*, 6(1), 28-36, 2018.

- **Presentations**

- A.Terracciano, A. Parupalli, Z. Loparo, J. Urso, S.S. Vasu, "Advancement of LED-based hazardous gas sensors for space applications." *2018 AIAA SPACE and Astronautics Forum and Exposition*. 2018.
- A. Terracciano, K. Thurmond, M.S. Villar, J. Urso, A. Parupalli, E. Ninnemann, Z. Loparo, N. Demidovich, J. Kapat, W. Partridge, S.S. Vasu, “Flight Test Demonstration of LED-based Fire Sensors for Space Propulsion Vehicles”, presented at the ESS/CI Spring Technical meeting, State College, PA, 3/2018.



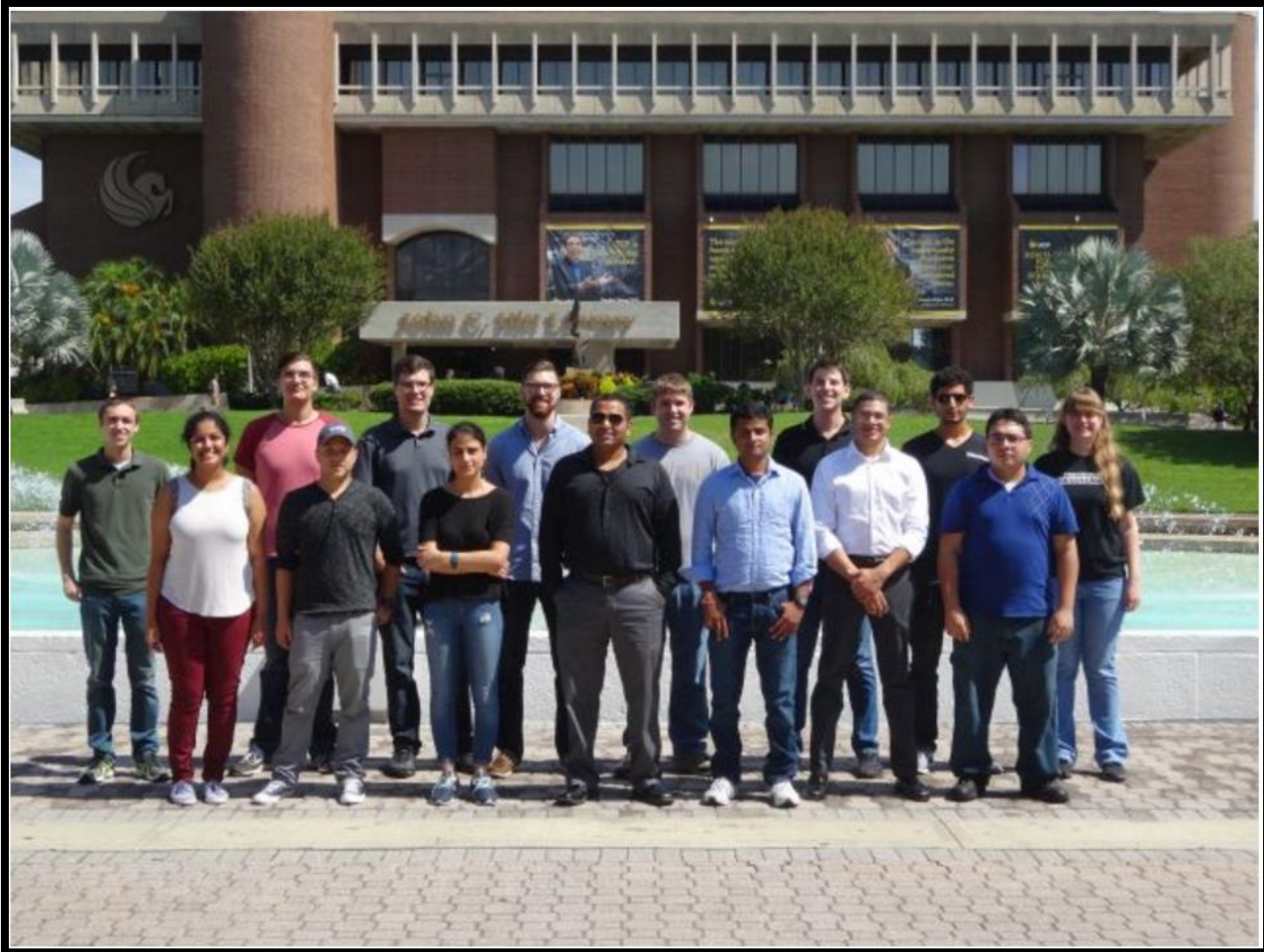
# Acknowledgements



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# Questions?



Vasu Lab 2016