

COE CST Fifth Annual Technical Meeting

Space Environment MMOD Modeling and Prediction

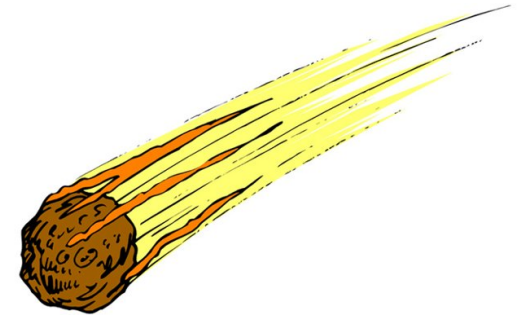
Sigrid Close and Alan Li
Stanford University

October 27-28, 2015
Arlington, VA



Outline

- **Team Members**
- **Task Description and Prior Research**
- **Goals**
- **Methodology**
- **Results**
- **Conclusions and Future Work**



Team Members

- **Sigrid Close, Stanford University (PI)**
- **Alan Li, Stanford University (graduate student)**

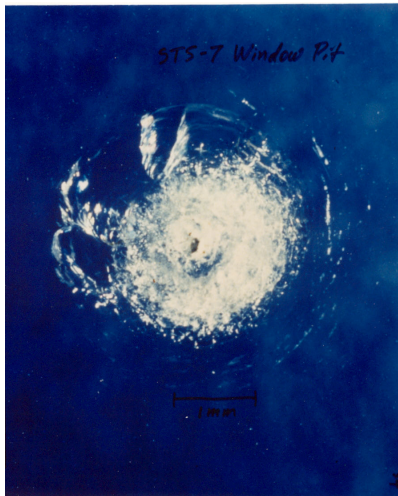


- **Lorenzo Limonta, Stanford University (graduate student supported by NSF)**



Purpose of Task

- **Spacecraft are routinely impacted by micrometeoroids and orbital debris (MMOD)**
 - Mechanical damage: “well-known”, larger (> 120 microns), rare
 - Electrical damage: “unknown”, smaller/fast, more numerous



- **Growing need to characterize MMOD down to smaller sizes and provide predictive threat assessment**

MMOD – Classification

- **Meteoroids**

- **Speeds**

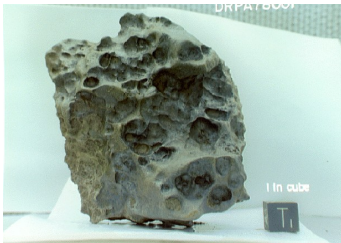
- 11 to 72.8 km/s (interplanetary)
 - 30-60 km/s (average)

- **Densities**

- $\leq 1 \text{ g/cm}^3$ (icy) or $> 1 \text{ g/cm}^3$ (rocky/stony)

- **Sizes**

- $< 0.3 \text{ m}$ (meteoroid)
 - $< 62 \mu\text{m}$ (dust)



- **Space Debris**

- **Speeds in LEO**

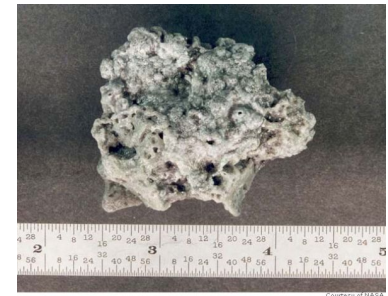
- $< 12 \text{ km/s}$
 - 7-10 km/s (average)

- **Densities**

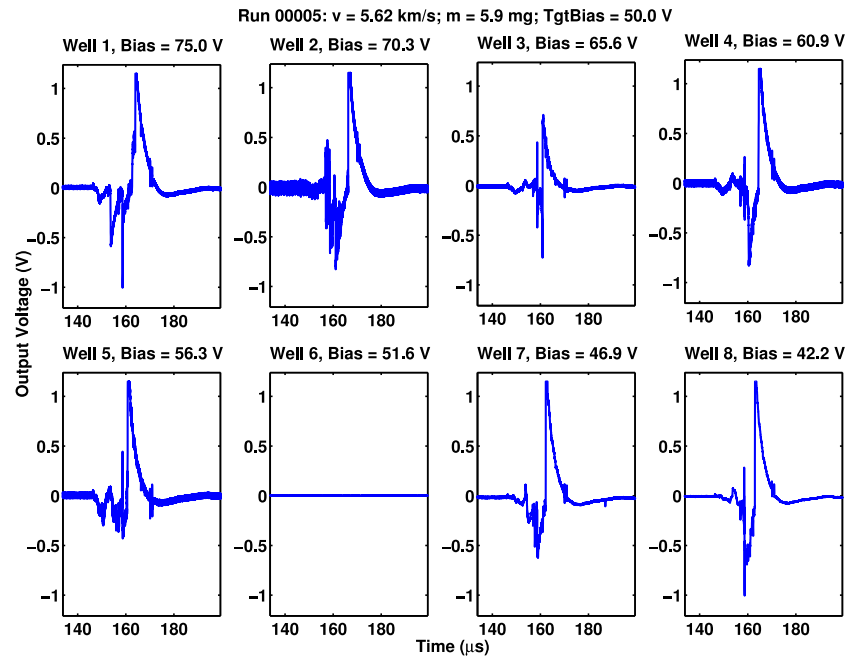
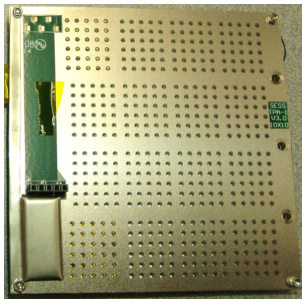
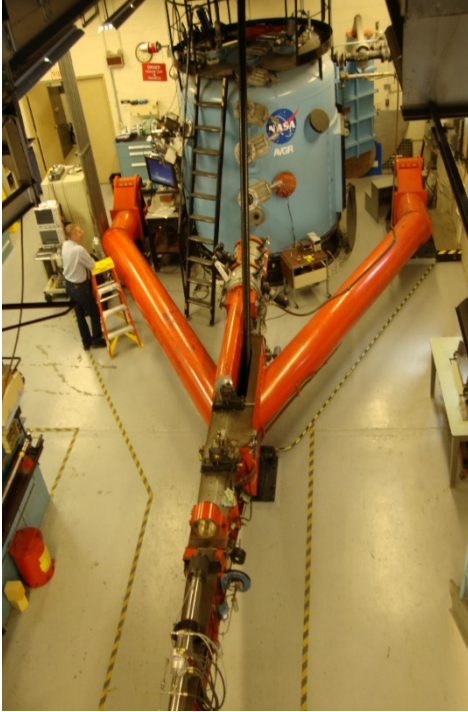
- $> 2 \text{ g/cm}^3$

- **Sizes**

- $< 10 \text{ cm}$ (small)



MMOD – Previous Research

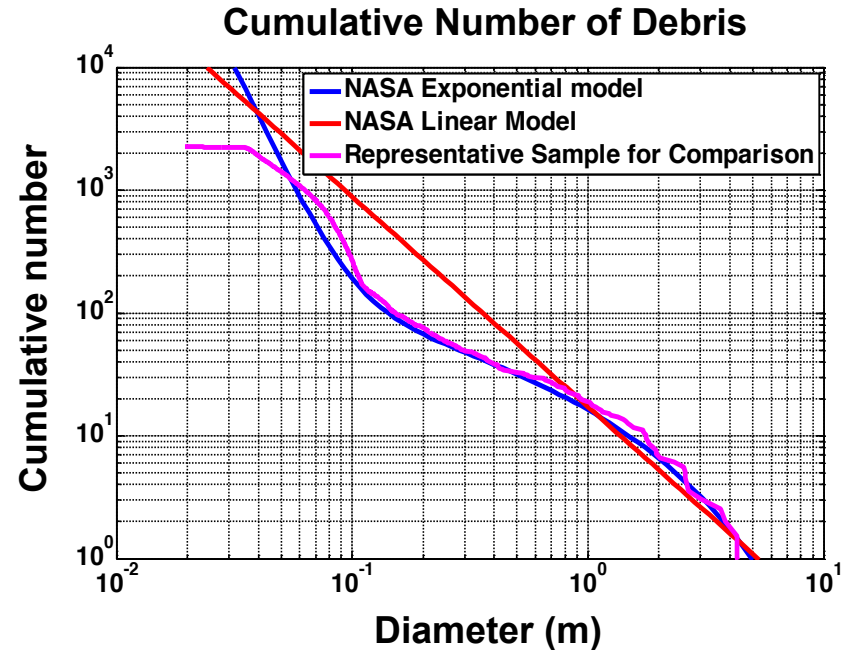


MMOD – Previous Research



- **EISCAT Svalbard radar**

- 78.1°N, 16.0°E
- 500 MHz, 32 m dish, 0.8 MW peak power
- Data collected March 2007 – March 2009 (following Chinese ASAT test in January 2007)



MMOD and Neutral Densities



- **“Space junk” WT1190F**
 - Approximately 1-2 m long
 - Most likely discarded rocket body “lost” by SSN
 - Reentry on November 13 (point of impact over Indian Ocean?)
- **Can we improve the 15-50% error?**

Goal: Neutral Density Estimation



Source: <http://eijournal.com/print/articles/entrepreneurial-blueprint-bolsters-satellite-development>



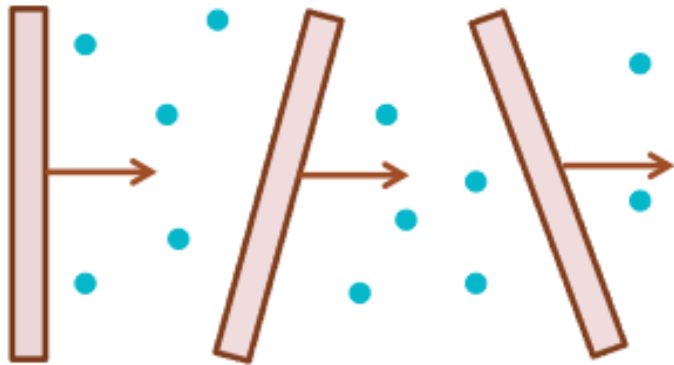
Source: http://www.huffingtonpost.com/2014/04/21/lyrid-meteor-shower-2014_n_5186204.html

- Leverage the increasing number of constellations of satellites in orbit
- Leverage the abundance of meteoroids ablating in the atmosphere
- Good temporally and spatially varying profile of neutral density
- Different source of density estimation

Methodology

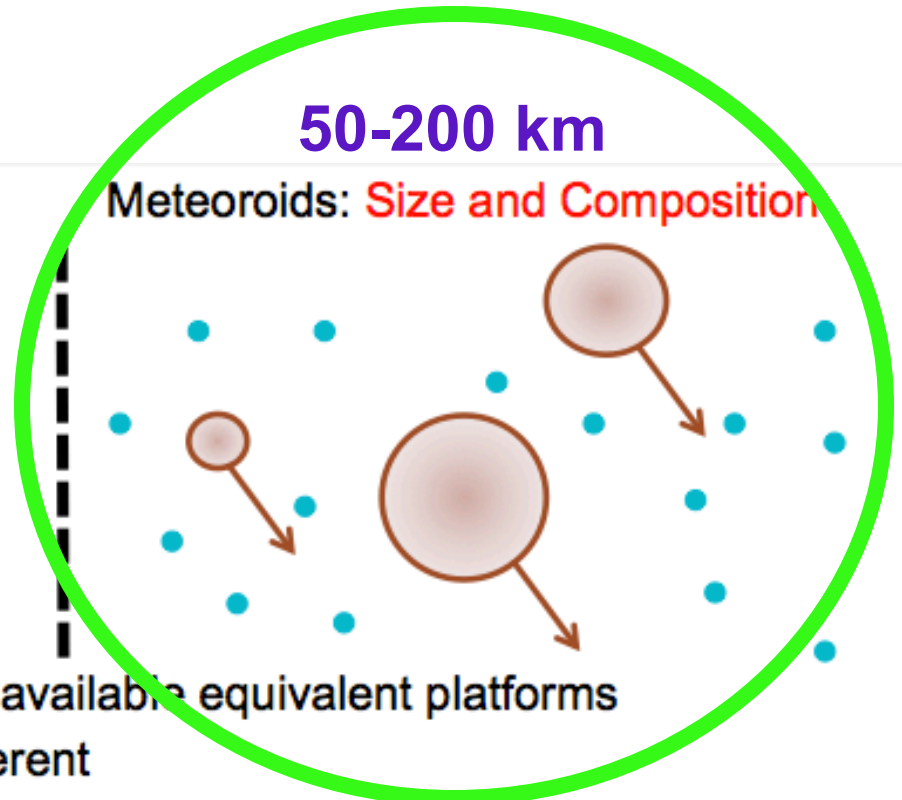
300-500 km

Satellites: Orientation



50-200 km

Meteoroids: Size and Composition



- Want to measure density from readily available equivalent platforms
- Each of these platforms is slightly different
- Measurements made at a certain time contains certain biases (across all platforms)

Data

Remove
Bias

Estimate
Variation

Calculate
Density

Assumptions and Equations

- **Assumptions**

- C_D constant (spherical shape)
- Variation arises from mass/size/bulk density
- Multiple layers of atmosphere traversed
- Ablation and mass loss

- **Governing equations**

Drag:
$$\frac{dv}{dt} = -\frac{3 \rho_a C_D}{8 \rho_m r} |v|^2$$

Ablation:
$$\frac{dr}{dt} = -\frac{1 C_H \rho_a}{8 H^* \rho_m} |v|^3$$

Velocity:	v	Enthalpy of Destruction:	H^*
Radius:	r	Coefficient of Heat Exchange:	C_H
Atmospheric Density:	ρ_a		
Meteoroid Density:	ρ_m		

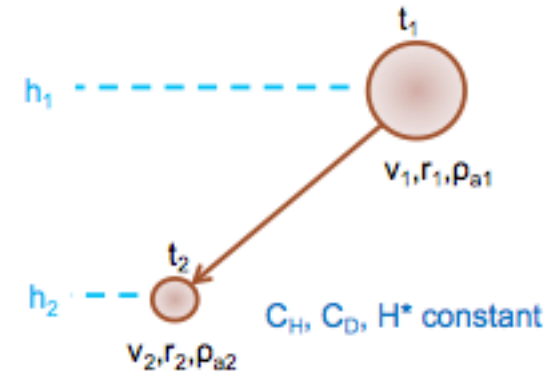
Density Ratios

- Combine drag and ablation equations and compare ratios of radii at different points in time

$$\frac{r_1}{r_2} = \exp\left(\frac{1}{6} \frac{C_H}{C_D} \frac{1}{H^*} (v_1^2 - v_2^2)\right)$$

- For i^{th} meteoroids at j^{th} altitude

$$\underbrace{\ln\left(\frac{dv_{i,j+1}}{dt} \frac{1}{v_{i,j+1}^2}\right) - \ln\left(\frac{dv_{i,j}}{dt} \frac{1}{v_{i,j}^2}\right)}_{\text{LHS}_i} = \underbrace{\frac{1}{6} D_i (v_{i,j}^2 - v_{i,j+1}^2) + \ln(\rho_{rj})}_{\text{RHS}_i}$$



- Given data on velocity and deceleration, estimate D_i and ρ_{rj} for each meteoroid and altitude

Minimize:

$$\min\left(\sum_{i,j} (\text{LHS}_{i,j} - \text{RHS}_{i,j})^2\right)$$

Subject to:

$$D_i > 0$$

$$D_i = \frac{C_{Hi}}{C_{Di}} \frac{1}{H_i^*}$$

$$\rho_{rj} = \frac{\rho_{a,j+1}}{\rho_{a,j}}$$

Ratio Distribution

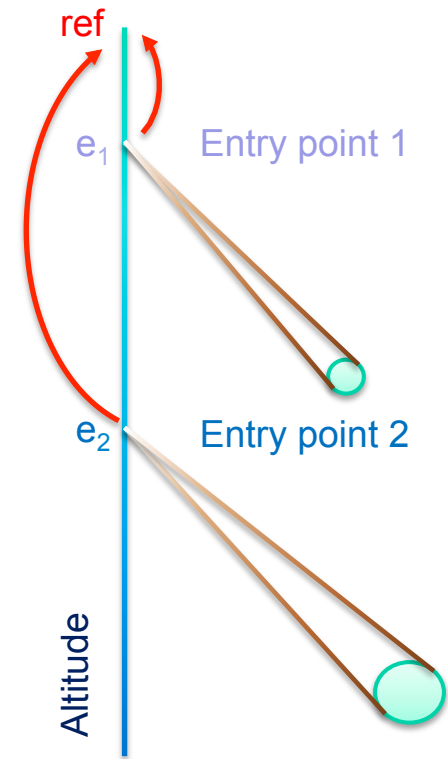
- Translate point of entry measurement to a reference point in altitude

$$\frac{dv}{dt} \frac{1}{v^2} \sim \frac{\rho_{a,e}}{r_e \rho_m} \longrightarrow \frac{dv}{dt} \frac{1}{v^2} \frac{\rho_{a,ref}}{\rho_{a,e}} \sim \frac{\rho_{a,ref}}{r_e \rho_m} = K$$

- Calculate K for each meteoroid and define minimum ratio using order statistics

$$\frac{K_j}{K_{mk}} \approx \frac{\left(\frac{1}{r_e \rho_m}\right)_j}{\left(\frac{1}{r_e \rho_m}\right)_{mk}}$$

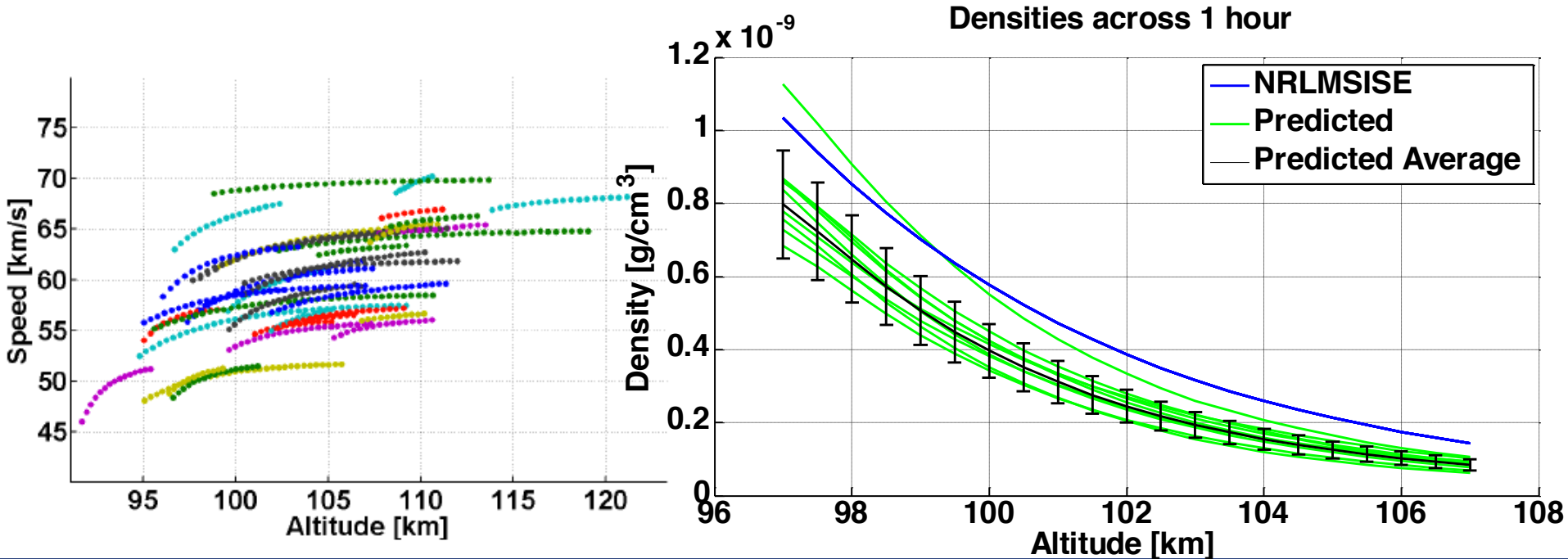
- Calculate distribution



Results

- **ALTAIR radar**

- 9°N, 167°E
- 160 and 422 MHz, 46 m dish, 6 MW peak power
- Data collected November 8th 2007 (6 AM local time)



Conclusions and Future Work

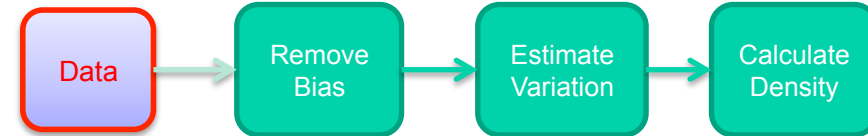
- **New method for estimating neutral density from multiple measurements across equivalent platforms**
 - Errors < 10% using CubeSats (not shown), 12% for meteoroids
 - Additional data to modeling community
- **Next steps**
 - Satellites: precision orbit determination
 - Meteoroids: ablation physics
 - Space debris: highly variable C_D

Li, A., and Mason, J. *Optimal Utility of Satellite Constellation Separation with Differential Drag*. 2014 AIAA/AAS Astrodynamics Specialist Conference. AIAA 2014-4112.

Li, A., and Close, S. *Mean Thermospheric Density Estimation derived from Satellite Constellations*. *Advances in Space Research* 56 (2015), pp. 1645-1657. DOI: 10.1016/j.asr.2015.07.022

Thank you!

Ballistic Factors



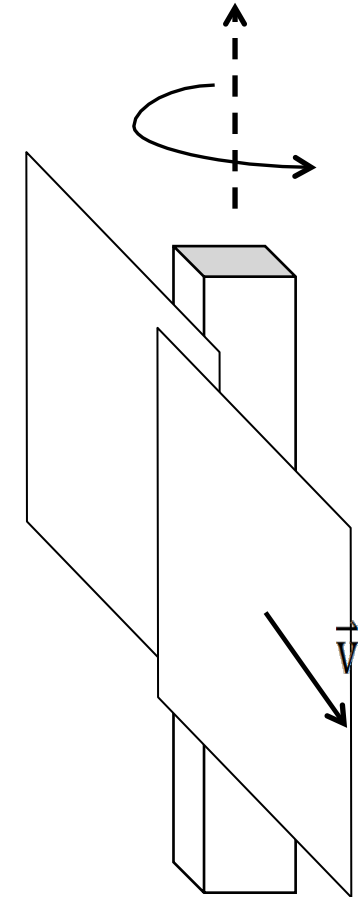
- θ : Rotation about the satellite spin axis (IID)
- Ballistic factor:

$$B(\theta) = \frac{C_D(\theta)A(\theta)}{m}$$

- › B is IID with some unknown distribution
- › B_{\min} defined when $\theta=0$ (absolute minimum)

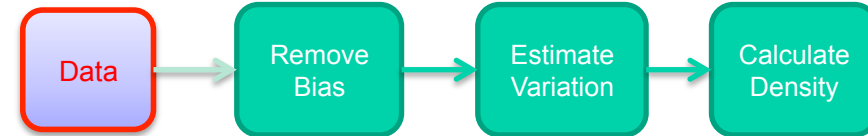
- Ignore rotations about other axes

$$B_{\min} = \frac{C_{D,\min}A_{\min}}{m}$$

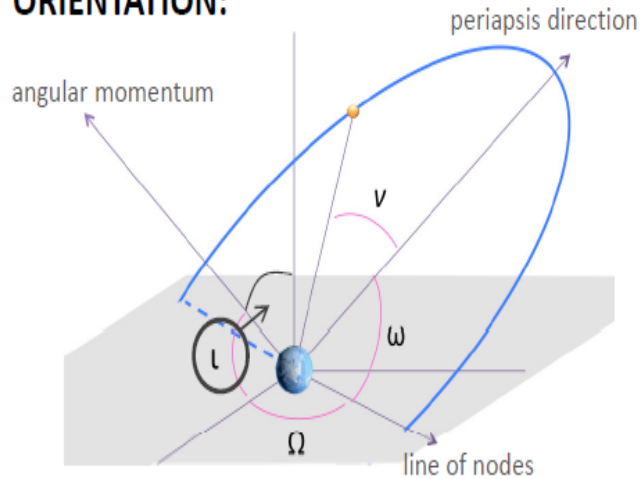


IID = Independent and Identically Distributed

Orbital Elements



ORIENTATION:



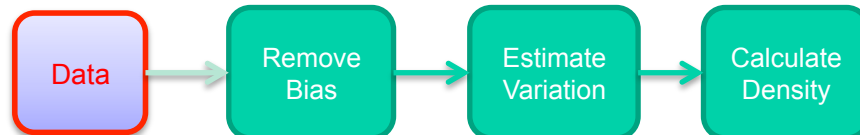
- Kept up to date by NORAD (Space-track)
- Uses Simplified General Perturbations (SGP) model
- Within few km of error over 1 day

Name of Satellite (11 characters)	International Designator	Epoch Year & Day Fraction	1st derivative of Mean Motion or Ballistic Coefficient	2nd derivative of Mean Motion, usually blank	Drag term or radiation pressure coefficient	Element Number & Check sum
NOAA 6	11416U 84123 A	86 50.28438588	0.00000140	00000-0	67960-4 0	5293
	11416	98.5105	69.3305	0012788	63.2828	296.9658
						14.24899292
						3646978

Labels for the second row of data:

- Satellite Number: 11416
- Inclination: 98.5105
- Right Ascension of the Ascending Node: 69.3305
- Eccentricity: 0012788
- Argument of Perigee: 63.2828
- Mean Anomaly: 296.9658
- Mean Motion: 14.24899292
- Revolution number at epoch & check sum: 3646978

Data



From TLEs

- $$\left. \frac{da}{dt} \right|_D = \frac{2a^2 v}{\mu} \frac{d\vec{v}_D}{dt} \cdot \hat{e}_v = \frac{2a^2 B v^3 F}{\mu}$$
- $$\Delta a_{SGP4}(t_i, t_k) = \int_{t_i}^{t_k} \left. \frac{da}{dt} \right|_D + \left. \frac{da}{dt} \right|_G + \left. \frac{da}{dt} \right|_U dt$$

small
- $$\Delta \bar{n}_M(t_i, t_k) = \frac{3}{2} \mu^{-\frac{2}{3}} \int_{t_i}^{t_k} \bar{n}^{\frac{1}{3}} \rho B v^3 F dt$$
- $$\bar{\rho} \bar{B} \cong \frac{2 \mu^{\frac{2}{3}} \Delta \bar{n}_M(t_i, t_k)}{3 \int_{t_i}^{t_k} \bar{n}^{\frac{1}{3}} v^3 F dt} = K$$

From ranging data

- $$\mathbf{X} = \begin{bmatrix} \mathbf{r} \\ \mathbf{v} \\ \mathbf{K} \end{bmatrix}, \mathbf{X}_0 = \begin{bmatrix} \mathbf{r}_0 \\ \mathbf{v}_0 \\ \mathbf{K}_0 \end{bmatrix}$$
- $$\dot{\mathbf{X}} = \mathbf{F}_D(\mathbf{X}) + \mathbf{F}_g(\mathbf{X}) + \mathbf{F}_U(\mathbf{X})$$
- $$\tilde{\mathbf{b}} = \mathbf{R}(\dot{\mathbf{X}}(t_i, \mathbf{X}_0)) - \mathbf{R}_{\text{meas}}(t_i)$$
- $$\delta \mathbf{x} = (\mathbf{A}^T \mathbf{W} \mathbf{A})^{-1} \mathbf{A}^T \mathbf{W} \tilde{\mathbf{b}}$$
- Loop until $\text{RMS} < \text{Threshold}$:
- $$\rightarrow \mathbf{X}_0 = \mathbf{X}_0 + \delta \mathbf{x}$$
- $$\text{RMS} = \sqrt{\frac{\tilde{\mathbf{b}}^T \mathbf{W} \tilde{\mathbf{b}}}{n_{\text{obs}}}}$$

How to Remove Bias

- Density estimated as:

$$\bar{\rho} \cong \frac{2\mu^{\frac{2}{3}}\Delta\bar{n}_M(t_i, t_k)}{3\bar{B}\oint_{t_i}^{t_k} \bar{n}^{\frac{1}{3}} v^3 F dt} = \frac{K}{\bar{B}} \quad \text{or} \quad \bar{\rho}\bar{B} = K$$

- K can be calculated by:
 - › SGP4 in the case of TLEs
 - › Ranging or GPS measurements; propagator needs to account for higher order gravity terms, SRP, etc...
- Internal bias within K because K is composed from varying densities

Ballistic factor:	$B = \frac{C_D A}{m}$
Mean motion:	n
Wind Factor:	F
Density:	ρ

The Dilemma: If we have N satellites, we have K_N measurements but need to estimate $n+1$ values (ρ and B_N), where B_N is randomly distributed

Order Statistics

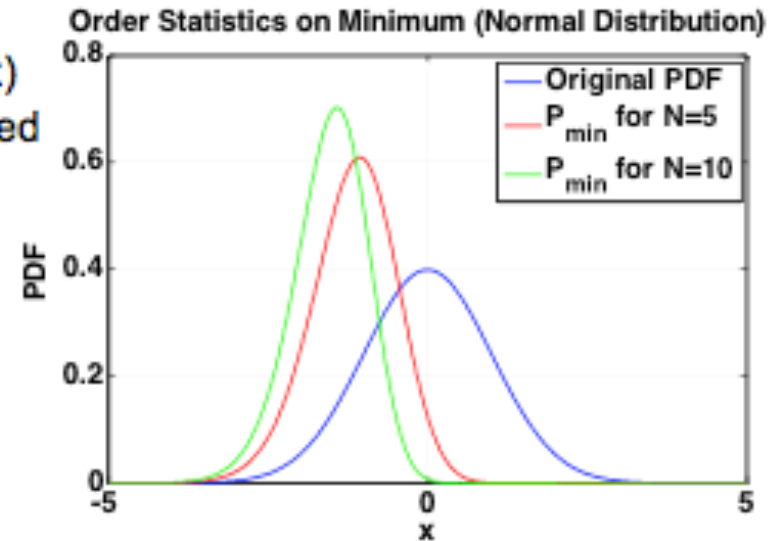
- What is order statistics?
 - › Let X_1, X_2, \dots, X_N be IID with some CDF $C(x)$
 - › Then the r^{th} order statistic can be expressed as:

$$C_{(r)}(x) = \sum_{i=r}^N \binom{N}{i} C^i(x) [1 - C(x)]^{N-i}$$

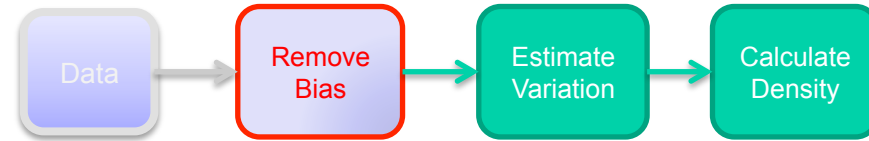
- › And the minimum as:

$$C_{(1)}(x) = 1 - [1 - C(x)]^N$$

- Why do we use it?
 - › We know something about the minimum of C_D from physics
 - › We have many satellites
 - › Estimation of C_D is difficult due to coupling with ρ



Remove Bias



- Define the minimum of our observations:

$$K_{mk}(t_k) = \min_j K_j(t_k)$$

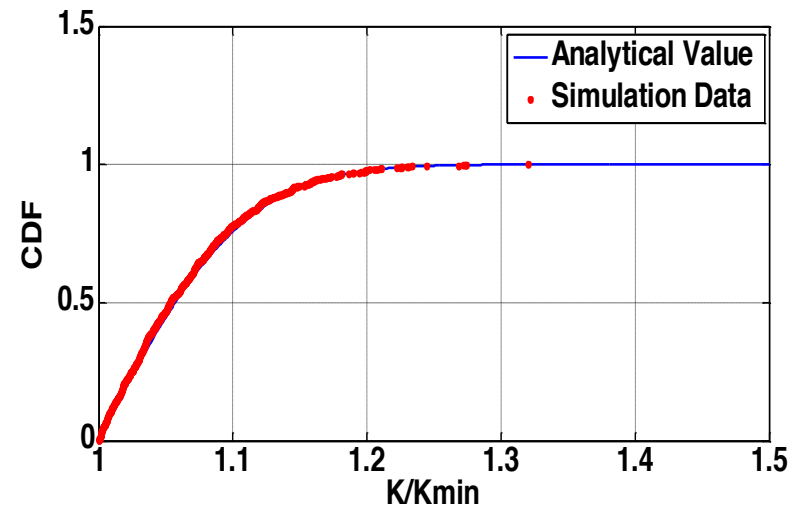
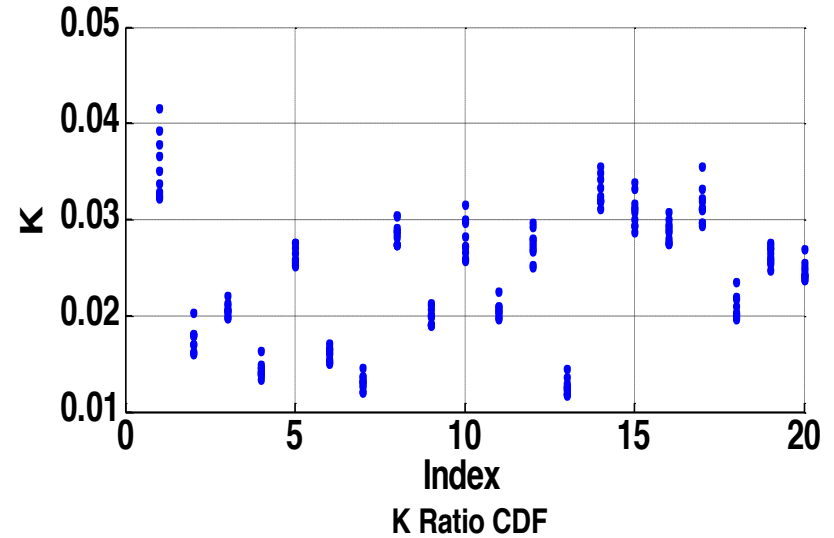
$$\frac{K_j(t_k)}{K_{mk}(t_k)} \approx \frac{B_j(t_k)}{B_{mk}(t_k)}$$

- Amalgamate measurements across all time periods to construct CDF ratio:

- Results in ratio distribution

$$CDF\left(\frac{B}{B_{mk}} \mid \frac{B}{B_{mk}} > 1\right)$$

Randomly distributed K



Ratio Distribution

- Probability of ratios defined as:

$$P(z) = \int_{-\infty}^{+\infty} |y| P_{B,y}(zy, y) dy$$

Math

$$C(z) = \frac{N}{N-1} \int_{B_{\min}}^{B_{\max}} F_B(z \cdot y) \cdot \frac{d(F_B^{N-1}(y))}{dy} dy + 1$$

Discretize

$$C(z_j) - 1 = \frac{N}{N-1} \sum_{i=1}^m F_B(z_j y_i) (F_B^{N-1}(y_{i+1}) - F_B^{N-1}(y_i))$$

- Limits:

$$\lim_{B \rightarrow B_{\min}} F_B(B) \rightarrow 1$$

$$\lim_{B \rightarrow B_{\max}} F_B(B) \rightarrow 0$$

$$y = B_{mk}$$

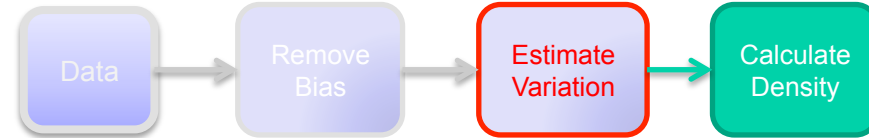
$$z = \frac{B}{B_{mk}}$$

$N = \#$ of platforms

$C_B = \text{CDF}(B)$

$F_B(B) = 1 - C_B(B)$

Discretization



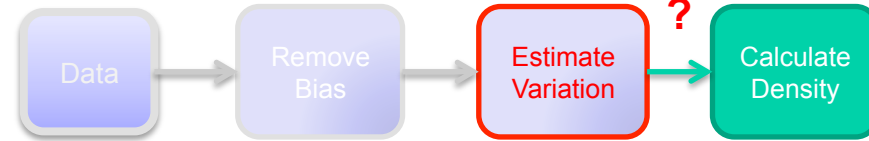
- Matrix form:

$$\underbrace{\frac{N-1}{N} \left(\begin{bmatrix} C(z_m) \\ C(z_{m-1}) \\ \vdots \\ C(z_2) \end{bmatrix} - 1 \right)}_{\text{LHS}} = \underbrace{\begin{bmatrix} F_{B,m} & 0 & \dots & 0 \\ F_{B,m-1} & F_{B,m} & \dots & 0 \\ \vdots & \vdots & \ddots & \vdots \\ F_{B,2} & F_{B,3} & \dots & F_{B,m} \end{bmatrix}}_{\text{Matrix}} \begin{bmatrix} F_{B,2}^{N-1} - F_{B,1}^{N-1} \\ F_{B,3}^{N-1} - F_{B,2}^{N-1} \\ \vdots \\ F_{B,m}^{N-1} - F_{B,m-1}^{N-1} \end{bmatrix}$$

- Minimize Subject to: $\min \left(\sum (\text{LHS} - \text{RHS})^2 + \kappa \cdot \max \left(\frac{dC_B}{dz} \right) \right)$

$$0 = F_{B,1} > F_{B,2} > \dots > F_{B,m} = 1$$

Effects of Error

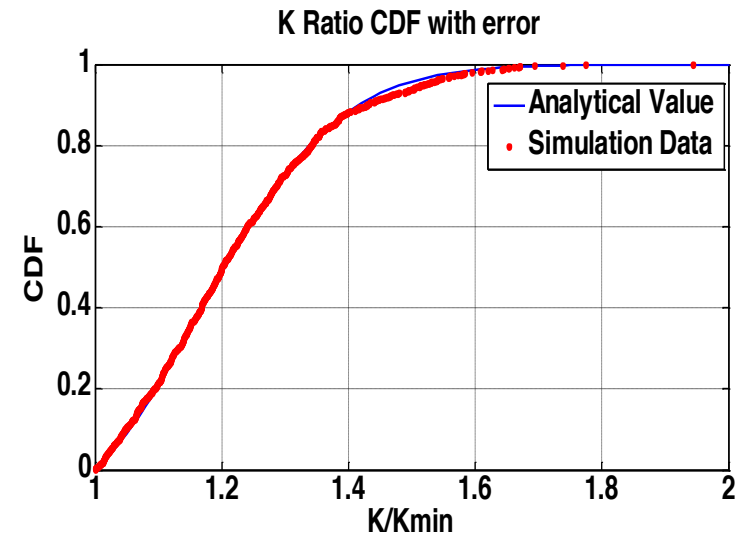
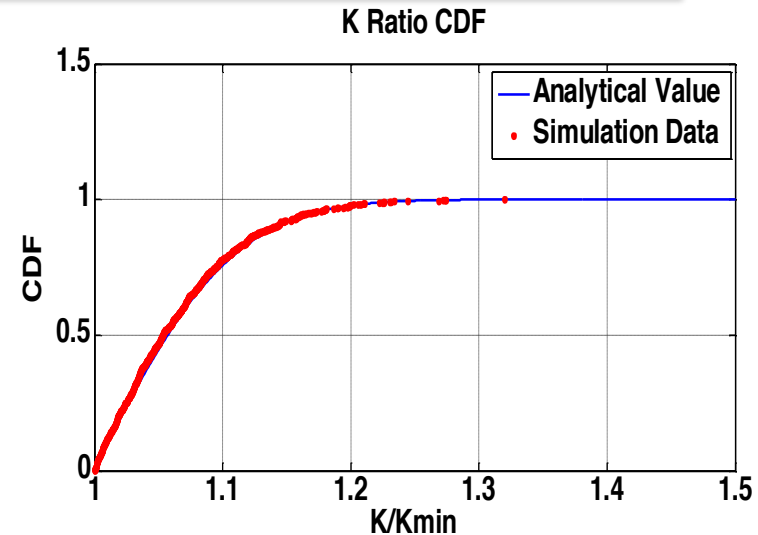


- Any estimation scheme is prone to error
- These errors affect the minimum ratio and hence its CDF

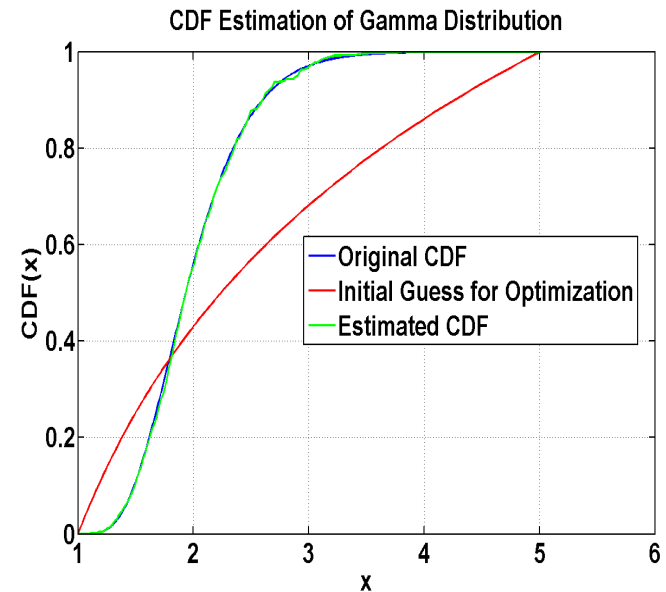
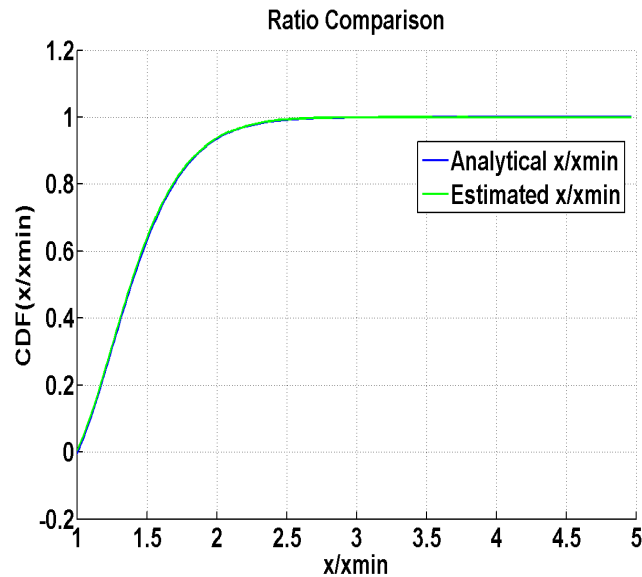
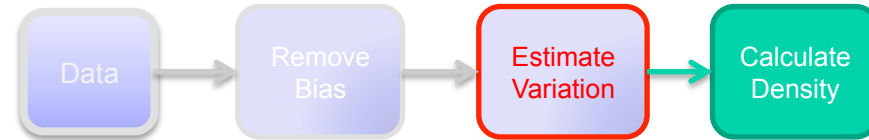
$$CDF \left(\frac{(B + dB)}{(B + dB)_{mk}} \mid \frac{(B + dB)}{(B + dB)_{mk}} > 1 \right)$$

- Estimate $(B + dB)$ using similar method
- Require statistics on the error of dB
 - › Estimate from previous filtering methods (non-linear least squares to estimate K)

$$dB \sim \mathcal{N} \left(0, \frac{\sigma_K}{\bar{\rho}} \right) \quad C_{B+dB}(X) = [C_B * P_{dB}](X)$$



Solving for F

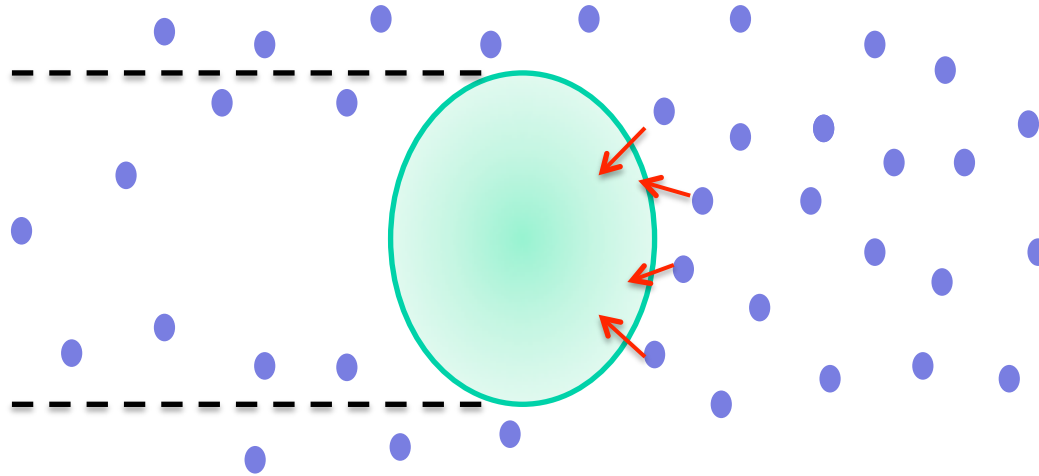
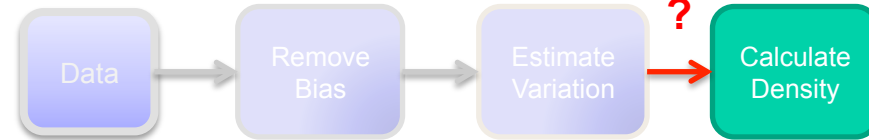


- Test Case: Gamma Distribution
-

Problem: If the distribution shifted left or right and is scaled appropriately, get same observed result (unknown integration constant)!

How to determine the minimum, B_{\min} ?

Free Molecular Flow



Mean free path:	λ
Characteristic length:	L
Number density:	N
Collision Area:	σ_A

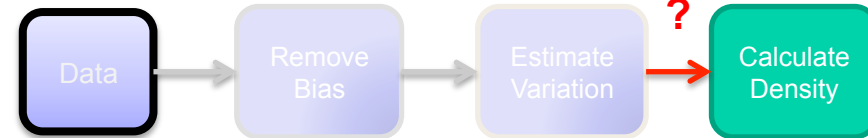
- Knudsen number: $Kn = \frac{\lambda}{L}$ $\lambda \sim \frac{1}{N\sigma_A}$
- High Knudsen numbers: Free molecular flow ($Kn \gg 10$)
 - › Basically collisionless, not a continuum (no bulk properties)
 - › Random thermal motions dominant: Maxwellian distribution

$$B = \frac{C_D A}{m}$$

min ↓

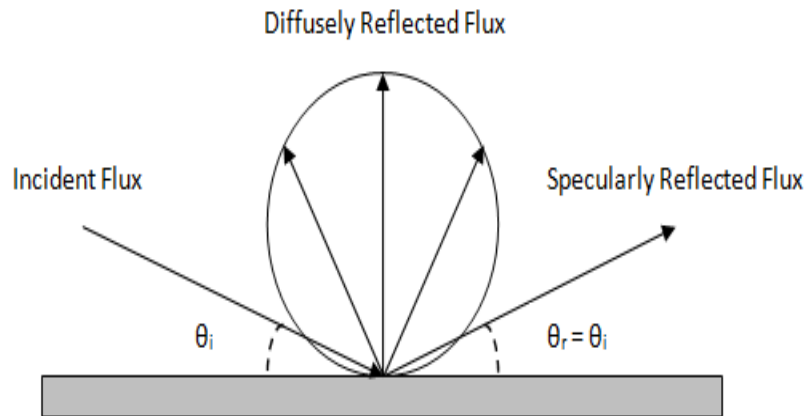
$$B_{\min} = \frac{C_{D,\min} A_{\min}}{m}$$

Free Molecular Flow



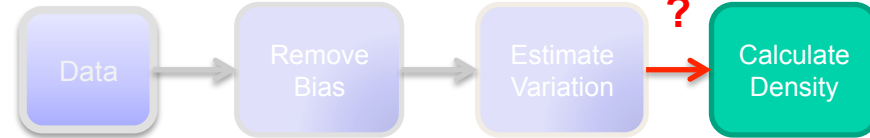
- Accommodation coefficient:

$$\alpha = \frac{E_i - E_r}{E_i - E_w}$$



- Reflected particles classified as:
 - › Specular – perfect reflection about surface normal
 - › Diffuse – random
- Surfaces for satellites in LEO tend to become coated with adsorbed atomic oxygen; most reflections are diffuse (80-99%)

C_D on Flat Plate

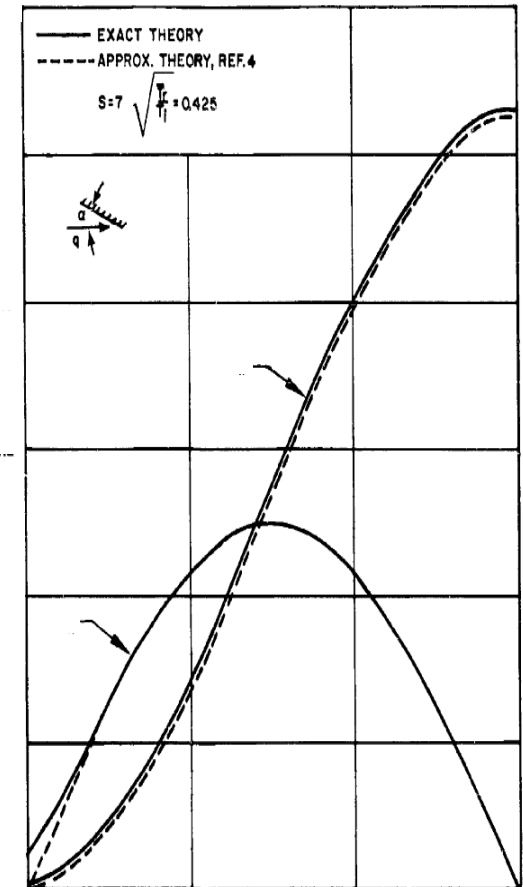


$$C_D = \frac{A}{A_{ref}} \left[(2 - \sigma_N) \cos \theta \left(\cos \theta (1 + erf(\gamma)) + \frac{1}{S\sqrt{\pi}} e^{-\gamma^2} \right) + \frac{2 - \sigma_N}{2S^2} (1 + erf(\gamma)) + \frac{\sigma_N}{2} \sqrt{\frac{T_r}{T_i}} \left(\frac{\sqrt{\pi}}{S} (1 + erf(S)) + \frac{1}{S^2} e^{-S^2} \right) \right]$$

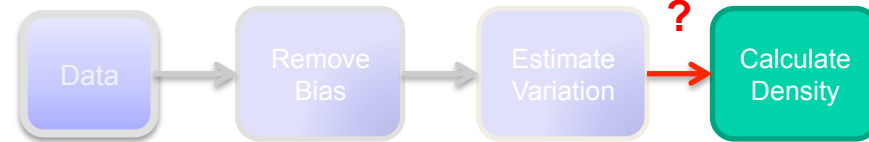
$$\gamma = S \cos \theta$$

$$T_r = T_i(1 - \alpha) + \alpha T_w$$

$$S = \frac{U}{V_a} = \frac{U}{\sqrt{2R_{sp}T_a}}$$



Uncertainty in α



- Combine this with earlier results:

$$P(B, \alpha) = P(B|B_{min})P(B_{min}|\alpha)P(\alpha)$$

- B_{min} is a function of α :

$$C(B) = \int_{B_{min,\alpha=1}}^{B_{max}} C(B|B_{min})P(B_{min})dB_{min}$$

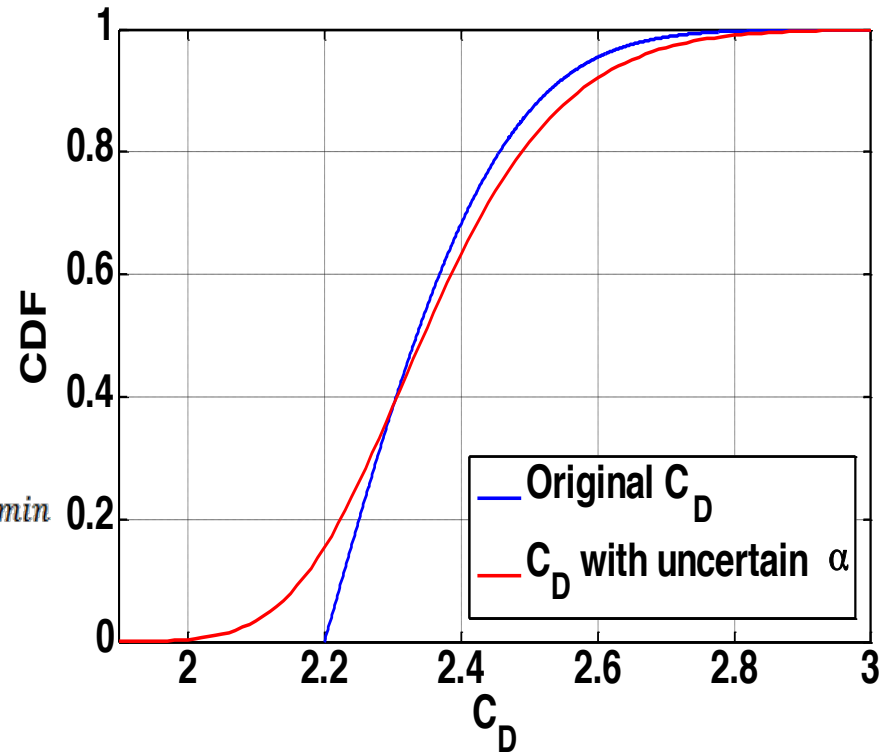
- Limits:

$$C(B_{mk}) = \int_{B_{min,\alpha=1}}^{B_{max}} C(B_{mk}|B_{min})P(B_{min})dB_{min}$$

$$\lim_{N \rightarrow \infty} P(B_{mk}) \rightarrow P_{min}$$



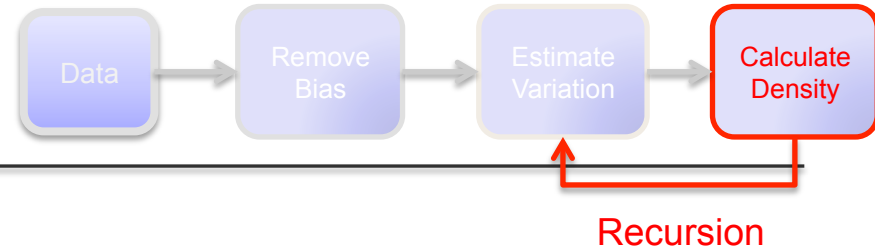
Effect of uncertain α



$C_D \sim$ Half Normal
0.1)

$\alpha \sim (2.2,$

Calculating Density



- Calculate density ρ :

Mean Estimate: $\rho_k = \frac{\bar{K}_k}{\bar{B}}$

- Minimum
- Maximum

K
B

Minimum Estimate: $\rho_k = \frac{K_{mk}}{\bar{B}_{min}}$

- Maximum
- Minimum

K_{mk}
 B_{min}

- K contains estimation error
- B contains error associated with platform
- Nullify large estimation errors in K from affecting estimation of B
-

Have to choose which one to minimize!

Separate estimation error from the random elements of the platform in question